Evaluation and Adjustment of Infrastructure Leakage Index

for Towns in Developing Countries

Geremew Sahilu Gebrie

School of Civil and Environmental Engineering, Addis Ababa Institute of Technology, Addis Ababa University, Addis Ababa, Ethiopia E-mail Address: geremew.sahilu@aau.edu.et

DOI: https://doi.org/10.20372/zede.v42i.10184

ABSTRACT

Evaluating water loss and the performance of urban water supply utilities is critical. The objective of this research was to applicability evaluate the of the Infrastructure Leakage Index (ILI) formula for towns of developing countries and suggest adjustment factors. Basic water supply data from nine towns of Ethiopia was used to calculate ILI and develop modification factors. Water supply development level factor was determined based on the actual water production and optimal consumption if there was sufficient supply. Asset management factor was developed considering the categorization of Ethiopian towns which was related to expected water supply level based on development level. The study showed the Unavoidable Annual Real Loss (UARL) formula gave similar values for any type of water supply system whether developed or not. Except for Addis Ababa, the calculated ILIs utilizing the standard formula were less than four indicating unrealistic very good performance. Applying the adjustment factors, realistic ILI values were obtained reflecting the realistic performance of water utilities in developing countries, requiring timely appropriate water loss reduction measures.

Keywords: Adjustment factors; Developing Countries; Ethiopia; ILI; Mode of water supply; Water loss.

1. INTRODUCTION

One of the major challenges of water supply service provision is the water loss between the production and end use points of a water supply system. A number of efforts were made to quantify the amount of water loss and develop key parameters that can be used to compare the performance of water utilities irrespective of their size with regards to population served and production The International capacity. Water Association (IWA) established a Task Force on Performance Indicators which published the standard international "best practice" water balance [1]. The water balance table which introduced the term Non-Revenue Water (NRW) has been used to assess the overall performance of the system with respect to percentage of water loss from a total production and also components of water loss such as apparent and real losses [2]. However, it was not suitable for assessing the efficiency of the distribution system as it was strongly influenced by consumption and its change and pressure; difficult to interpret for intermittent supply and couldn't distinguish between apparent loss and real loss [3].

The IWA's task force on water loss carried out a review of performance indicators for real losses [4] and developed a method that could represent most of the above factors by introducing the concept of UARL and Current Annual Real Loss (CARL) to calculate a dimensionless key performance parameter – ILI. IL I was calculated as ratio: CARL/UARL, Restegari [5] stated that the UARL/ILI approach was better than previous traditional performance indicators for the management of real losses. The basic concept of UARL was that there is no as such zero real loss. Figure 1 shows that if the real loss is to the left of point 'A', which is UARL, the cost of active leakage control will not be economically affordable [6]. Thus, the CARL should always be to the right of point 'A' in perfect condition at 'A' implying ILI greater than or equal to unity implying values closer to one mean good performance.



Figure 1 Unavoidable Annual Real Losses and Economic Level of Real Losses [6]

Equation (1) was developed by the task force to determine UARL (liters/day) taking into account most of the factors that were not addressed in the traditional performance indicators.

UARL = (18Lm + 0.80Nc + 25Lp)P (1)

where:

Lm= Mains length in km Nc = Number of service connections Lp = Total length in km of underground pipe between the edge of the street and customer meters

P = Average operating pressure in meter

In the development of ILI as a performance indicator to measure the efficiency of water utilities, the basic assumption in determining UARL was utilities will carry out four necessary measures of asset management

practice setting standard level of services (LOS) – pipeline and asset; and pressure management, active leakage control and speed and quality of repairs [7]. As mentioned by Alegre et al [8], the ILI was the result of an empirical expression considering properly constructed and maintained system having the service connection density, average length and the same average operating pressures. It was also mentioned that the indicator doesn't fulfill some of the requirements set for performance indicators. The ILI didn't have a means to consider developmental level of a water supply system. Modifying UARL equation for developing countries to calculate realistic ILI was also discussed by water leakage researchers [9].

Therefore, considering that the ILI was developed based on well-developed water supply systems and utilities the question here was, would such indicator give reasonable values for developing countries? Hence, the first objective of this paper was to check whether the ILI method could give reasonable performance assessment of water utilities in developing countries. The second objective was to recommend adjustment factor to the formula so that the result could reflect the situation of utilities in developing countries.

2. METHODS

The study focused on nine towns shown on Figure 2 including Addis Ababa, which is the only metropolitan city with a population of more than a million.



Figure 2 Location map of study towns in Ethiopia

The key formula and data used to determine the ILI and modification factors to make it applicable to the assessment of the performance of water utilities in developing countries is presented in the following subsections. The data were extracted with proper quality checking from project documents and graduate thesis works supervised by the author.

ILI Calculation

The towns and key basic data utilized for the calculation of the relevant parameters in the determination of ILI are presented in Table 1.

Table 1 Basic water supply system data of nine towns in Ethiopia

			Production	Billed Consumption	Length of Main (Lm)	System Average Pressure	Number of Connections
Town	Year	Population	(m ³ /day)	(m ³ /day)	(km)	$(\mathbf{P})(\mathbf{m})$	(Nc)
Addis Ababa	2012	3,000,000	307,328.08	184,472.88	2,840.00	25.00	298,900.00
Adama	2014	308934	18,496.88	12,194.47	410.00	35.00	36,226.00
Mettu	2015	46,306	1,211.67	791.98	20.92	38.43	3,109.00
Emdibir	2017	20,773	512.75	404.96	21.73	32.00	1,100.00
Wolkitae	2016	78,189	2,219.60	1,779.15	109.00	55.80	6,909.00
Debre Markos	2014	9,2470	3,809.62	2,292.93	55.72	43.00	11,014.00
Robe	2016	80,504	2,255.07	1,686.47	60.06	52.00	8,236.00
Bedeno	2016	13,418	388.80	311.04	10.31	25.00	366.00
Ginchi	2018	53,600	829.00	488.18	24.72	52.00	2,472.00

Sources: [10 -17]

When utilizing the basic data, some assumptions were made to determine CARL UARL employing the formulas v. and developed by the IWA taskforce and get the ILI for each town. The various parameters developed in the process of determining ILI with the ones utilized during the development of the ILI formula were compared with coefficient of determination vi. (R^2) and a separate data from Addis Ababa vii. Water and Sewerage Authority (AAWSA) branch offices was used to validate some of relationships the developed between UARL's and density of customer connections. The key parameters determined and used to determine the applicability of ILI in the study towns were:

- i. UARL=(18Lm + 0.80Nc + 25Lp)P; (liter/day) (1)
- ii. UARL: liter/connection/day(i/Nc)
- iii. UARL: liter/connection/day/meter of pressure (ii/P)

- iv. UARL: liter/km of Main/day/meter of pressure (i/Lm/P)
- CARL: Current Actual Real Loss (75 % of NRW) based on estimation of apparent losses and known values of measured and not measured consumptions which ranges from 20 % to 30% (average 25 %) gives a real loss of 75 % of NRW

Density of connection = Nc/Lm

ILI: CARL/UARL

The UARL value of each town was calculated utilizing equation 1 and data in Table 1.

Technical Performance

A physical loss assessment matrix, presented in Table 2, that sets technical performance category considering ranges of ILI values based on physical loss in liter/connection/day when a system is pressurized from 10 m to 50 m that was developed by Liemberger et al. [18] for developing countries was used to determine performance levels based on calculated ILI values. This was done before and after adjustment of ILI values to check the change in technical performance category.

Water quantity

Another set of data focusing on water production, billed water consumption and NRW in liter per capita per day (l/c/d) and percentage of mode of water supply connections is presented in Table 3 based on the data on Table 1 and additional regarding connections. This was used to determine modification factor based on water supply development level that depends on the quantity of water used to adjust the ILI in order to make it applicable for developing countries.

Table 2 P	hysical lo	ss assessment	matrix for	r developing	countries [18]
I UDIC # 1	iny sieur io	ss assessment	matrix 10	i developing	

Technical		Liters	Liters/connection/day when the system is pressurized							
Performance Category	ILI	10m	20m	30m	40m	50m				
А	1-4	<50	<100	<150	<200	<250				
В	4-8	50-100	100-200	150-300	200-400	250-500				
С	8-16	100-200	200-400	300-600	400-800	500-1000				
D	>16	>200	>400	>600	>800	>1000				

Table 3 Wate	r production.	billed consum	ption and NRV	V and	percentage of modes	of water supply	v in study	towns
I ubic o mult	n production.	, onica consum	iption and i tit	, and	percentage of modes	or water suppr	y m bluey	10 11 110
	1 7		1					

	Water	Billed water		House	Yard	
	production	consumption	NRW	Connection	Connection	Public
Town	(l/c/d)	(l/c/d)	(l/c/d)	(%)	(%)	Tap (%)
Addis Ababa	102.44	61.49	40.95	34.00	60.00	6.00
Adama	59.87	39.47	20.40	5.00	60.00	35.00
Mettu	26.17	17.10	9.06	2.20	43.80	25.00
Emdibir	24.68	19.49	5.19	0.38	64.89	20.99
Wolkitae	28.39	22.75	5.63	7.00	93.00	0.00
Debre Markos	41.20	24.80	16.40	3.00	25.00	39.00
Robe	28.01	20.95	7.06	3.12	59.28	37.60
Bedeno	28.98	23.18	5.80	0.00	15.00	85.00
Ginchi	15.47	9.11	6.36	2.96	51.57	34.66
Average	39.47	26.48	12.98	6.41	52.50	31.47

Asset management

In Ethiopia, the category of the town in addition to population size reflected the stage of water supply development with respect to service delivery which is highly affected by availability of a systematic asset management. The asset management was reflected by activities which are being carried out by water utilities to provide safe water satisfying standard LOS which includes in general decreasing NRW and particularly water loss. In the Ethiopian context, as per the second growth and transformation plan (GTPII), towns are categorized based on population into the following five categories [19]:

- Category I: > 1,000,000
- Category II: 100,000 to 1,000,000
- Category III: 50,000 to 100,000
- Category IV: 20,000 to 50,000
- Category V: < 20,000

This categorization which indicates the expected l/c/d of water supply of each category as 100, 80, 60, 40, 20 for categories I, II, III, IV and V, respectively was used to estimate asset management factor.

The water quantity and asset management factors were multiplied to determine modified ILI value which better reflects the performance level of the utilities in the study towns.

3. RESULTS AND DISCUSSION

3.1 Results

3.1.1 Pressure and Density of Connection

The first comparison was made between the UARL estimated (liter/connection/day) utilizing the field data and the table

produced by the developers of the formula based on data from 27 countries [6], as shown in Table 4. The field values of average pressure and density of connection per km of main were taken and the UARL was interpolated from the table. For density values greater than 100 Nc/km, UARL values corresponding to 100 Nc/km were taken as values become almost constant as observed from the table developed to estimate UARL during the ILI formula development [4].

Table 4 UARL values calculated based on field data and interpolated initial ILI document (liter/connection/day))

	Addis					Debre			
Town	Ababa	Adama	Mettu	Emdibir	Wolkitae	Markos	Robe	Bedeno	Ginchi
UARL Field	33.65	48.26	49.81	48.98	81.41	54.44	67.93	42.05	70.46
UARL Interpolated	31.00	44.05	47.11	45.45	84.71	45.15	66.30	40.04	66.30

The coefficient of determination (\mathbb{R}^2) value of 0.968 for estimated values of UARL based on field data and interpolated based on initial ILI document presented in Figure 3 shows that the table can directly be used to calculate UARL as long as the basic data in ILI equations are available. The estimation has reasonable accuracy and this indicates that the developed table can be used irrespective of the level of the water supply system of the data source.



Figure 3 UARL - Field value as a function of tabular values [6]

3.1.2. UARL per Unit Pressure

During the development of the ILI method, graphs were developed which showed the relationship between density of service connections per km and UARL: in liter/kmmain/day/meter of pressure and liter/connection/day/ meter pressure when fully pressurized [6]. The developed graphs show density increases UARL as (liter/connection/day/meter pressure) decreases and becomes almost constant if the density of connection exceeds 100 Nc/km. Moreover, the UARL (liter/km of main/day/meter pressure) increases linearly with density of connection except when considering only the main which is constant. Figures 4 and 5 were developed for the nine towns based on field data.

Comparison of the graphical representation of the source document for ILI method and the one plotted for the nine showed that the trends were similar in that UARL – liter/connection/day decreased with increase in density of service connection and vice





The equations developed to calculate UARLs per unit pressure based on the density of service connection in Figures 4 and 5 needed to be validated. The data for seven branch offices of AAWSA and calculated density and UARLs based on the data and developed equations as shown in Figures 4 and 5 are presented in Table 5. An average pressure of 25 meter is used as suggested in the Water Audit and Bench Marking Report [20].

 Table 5 Water distribution system data, calculated density and UARLs of AAWSA Branch offices and estimated values based on developed equations

UARL UARL Calculated based on data ² Calculated based on equilibrium	uation ³
Calculated based on data ² Calculated based on equilibrium	uation ³
	liter/km
	IIIUI/KIII
(liter/connection (n	main)/day)
(liter/conne (liter/km /day)/meter of /m	neter of
AAWSA Density ction/day/ (main)/day/ pressure) pr	ressure
Branch Lmain Lp^1 (Nc/km meter meter $(y = 2E-05x^2 - (y = $	y = 1.175x
OfficeNc(km)(km)(main)pressure)pressure) $0.0072x + 1.8655$ +	18)
Addis	
Ketema 40693 233.04 542 174.62 1.24 215.84 1.22 22	23.18
Arada 22317 219.91 307 101.48 1.32 134.09 1.34 134	37.24
Gulele 41841 274.23 665 152.58 1.32 200.69 1.23 19	97.28
Gurd Shola 32955 333.41 391 98.84 1.28 126.39 1.35 13	34.14
Megenagna 28580 235.12 337 121.55 1.24 151.08 1.29 16	60.83
Mekanisa 38066 270.97 534 140.48 1.28 179.65 1.25 18	83.06
Nifas Silk 39864 316.72 569 125.87 1.30 163.61 1.28 16	65.89

Calculated based on:

¹Lpranging from 12 m to 16 m is used source being bench marking report ²Equation 1 $3E_{12}$

³Equations of Figures 4 and 5

The RMSE of UARL (liter/connection /day)/meter of pressure) determined based on field data and developed equation is 0.0476 which is insignificant. Moreover, the

coefficient of determination (R^2) between UARL (liter/km(main)/day/meter pressure) determined through field data and developed

equation was 0.9834. Both validate the equations developed in Figures 4 and 5.

3.1.3 Infrastructure Leakage Index

The key parameter used to determine ILI was CARL which was calculated considering 75 % of the NRW based on the estimation of the apparent losses and unmetered and metered unbilled water consumption to be 25% of NRW. Table 6 shows the ILI calculated according to a formula: ILI = CARL/UARL.

Table 6 Calculated ILI for Ethiopian towns based onfield data indicated in table 1.

	CARL	UARL	
	(liters/conn	(liters/conn	
Town	ection/day)	ection/day)	ILI
Wolkitae	47.81	81.41	0.59
Robe	51.78	67.93	0.76
Emdibir	73.49	48.98	1.50
Mettu	101.24	49.81	2.03
Debre			
Markos	103.28	54.44	1.90
Ginchi	103.40	70.46	1.47
Adama	130.48	48.26	2.70
Bedeno	159.34	42.05	3.79
Addis			
Ababa	311.06	33.65	9.24
Average	120.21	55.22	2.66

In general, it is clear that increased CARL coupled with decreased UARL results in increased ILI. Comparing average values of CARL of Ethiopian towns with that reported by Lambert et al. [6], it was less than half -120 against 270 liter/connection/day and corresponding ILI was 2.66. If Addis Ababa is taken out, the average value of the CARL towns of eight is about 96 liter/connection/day while ILI is 1.84. Except for Addis Ababa, all calculated ILI values were less than 4 including less than one values for Wolkitae and Robe towns.

The ILI for the towns of *Emdibir*, Metu, *Ginchi* and *Bedeno* were considered though,

Nc, is less than 5,000 as most of the towns in developing countries have such nature and checking the applicability of ILI is necessary

Technical performance category

The technical performance category of a utility was determined assuming pressurized system by considering the ILI range, average pressure in the system and the extent of the current actual real loss [21]. The physical loss matrix developed for developing countries was used to categorize the 9 towns as presented in Table 7. Based on the parameters presented in the table, all but Addis Ababa were in the technical performance category of A. This category represents the ultimate good performance where further loss reduction may be uneconomical unless there was shortage of water, which needs careful analysis to cost-effective improvement identify measures. In the case of Addis Ababa, the technical performance category is C which is poor and requires immediate asset management and leakage control actions.

3.1.4 Modification factor

The technical performance category of A in Table 8, except for Addis Ababa, required attention. The question here was what was the situation on the ground in the various utilities that have registered performance category of A. Do they deserve such highlevel technical performance? Does it mean these utilities do not need further leakage control activities? Though developed for developing countries, can one really utilize this table to categorize technical performance in developing countries like Ethiopia? What modification is required to realistic technical performance get measurement? Considering the situation on the ground, there was a need to develop factors to modify calculated ILI.

	System Average Pressure	Infrastructur e Leakage	CARL (liter/connec	ILI-	CARL-	Technical Performance
Town	(P) (m)	Index (ILI)	tion/ day)	Range	Range	Category
Addis Ababa	25.00	9.24	311.06	8 - 16	200 - 400	C
Adama	35.00	2.70	130.48	1 - 4	< 150	А
Mettu	38.43	2.03	101.24	1 - 4	< 150	А
Emdibir	32.00	1.50	73.49	1 - 4	< 100	А
Wolkitae	55.80	0.59	47.81	<1	<50	А
Debre						
Markos	43.00	1.90	103.28	1 - 4	<150	А
Robe	52.00	0.76	51.78	<1	<100	А
Bedeno	25.00	3.79	159.34	1 - 4	<200	A
Ginchi	52.00	1.47	103.40	1 - 4	< 150	A

Table 7 Technical performance category of water supply utilities in study towns of Ethiopia

Water quantity perspective

The per capita water production, billed consumption, NRW and mode of water supply of the various utilities can be referred from Table 3. The average per capita production per day was about 40 liters while the billed consumption was just over 26 liters. If Addis Ababa is treated separately the average per capita production and consumption in liters will be about 32 and 22 liters, respectively which is very minimal.

The minimal consumption of water is reflected in the percentages of mode of water supplies in the towns with very low water consumption levels. A very low percentage of house connection of about 6.5% indicates that the maximum per capita water consumption is governed mainly by yard connection, 52.5 %, which could not be greater than 50 l/c/day. The fact that on the average about 32 % fetch water from public tap with a maximum possible daily per capita consumption of 20 liter justifies the low daily per capita consumption rates.

If Addis Ababa is not considered, the house connection, yard connection and public tap users will be about 3 %, 52 % and 35 %,

respectively. Considering similar average pressure and NRW, if the production amount is increased, CARL will increase. However, UARL will remain the same since it is not a function of water production or consumption as the key parameters in the equation are pipe length, number of connection and pressure. The UARL could not differentiate whether the water supply system is highly developed with most population house connected or yard connected or get water from the public taps.

The key implication of the lesser production and insignificant percentage of house connection and hence less CARL coupled with unchanged UARL is that the ILI will be lower. The issue here is to determine a correction factor which is greater than one for the calculated ILI to cater for the development level of water supply system. Considering the factor to be determined the adjusted ILI can be calculated as follows:

$$ILI_{adj1} = WSDLF*ILI$$
(2)

where:

ILI_{adj1}= Adjusted ILI considering the development level of water supply

ILI= ILI determined with available water assuming system is fully pressurized

WSDLF= Water Supply Development Level factor used to adjust ILI

Asset Management Perspective

Initially the ILI was developed considering utilities have proper asset management to achieve a certain level of service (LOS) which includes active leakage management practice. A recent study carried out in 10 small and medium towns of East Shoa Zone of Oromia region of Ethiopia [22] showed the following key technical factors which can be considered common problems in almost all towns of Ethiopia.

- the consumption was low due to underdevelopment of the system coupled with NRW which is a big concern and poor management,
- Infrastructure stability was also one attribute with low achievements of the evaluation in which many of the physical assets were found aged and needs replacement and repair; regular inspection periods were missed
- Product quality was very low expressed as service reliability, continuity, interruptions, working hours, and quality of water

Considering the nine towns with regards to asset management, the situation is not different. For example, in Debre Markos town 11.5 burst/km/year of main per year was encountered which clearly shows very poor asset management of the water supply system. Except Addis Ababa which started limited efforts on NRW management, other towns do not have proper asset management that leads to leakage control.

ILIadj2 = AMF*ILI(3)

where,

ILIadj2 = Adjusted ILI considering lack of proper asset management

ILI= ILI determined with available water assuming system is fully pressurized

 $ILIadj = AMF^*WSDLF^*ILI$ (4)

where:

ILIadj=Adjusted ILI considering lack of proper asset management and low water supply development level

ILI=ILI determined with available water assuming system is fully pressurized and proper asset management practiced

WSDLF=Water Supply Development Level Factor used to adjust ILI

Determining Adjustment Factors

Water Supply Development Level Factor (WSDLF)

Water supply development factor can be determined on assumed per capita daily water demand if a substantial population of the urban population is getting water through house connection. The WSDLF is basically determined considering the per capita production should be between 100 l/c/d to 150 l/c/d where more than 80 % of the population is utilizing water from house connection including NRW was considered as optimal. In this study a per capita production of 125 l/c/d which is an average of the two was considered to calculate WSDLF. The factors developed and the resulting adjusted ILI is presented in Table 8.

Asset Management Factor (AMF)

The category of the town in the asset management perspective section in addition to population size reflects the stage of water supply development with respect to service delivery which is highly affected by availability of a systematic asset management. Hence, depending on the status of asset management, correction factors that vary from 1.25 to 2.0 have been assigned. The maximum factor is given this range since the level of development with respect to asset management within Ethiopia or other developing country could not be more than double from the best scenario which is one. Otherwise, it can exaggerate the ILI value unnecessarily downgrading technical performance. The minimum AMF was assigned for Addis Ababa as it has a system in place but not that much effective since significant reduction in leakage is not vet observed. Adama is just beginning the introduction of the system with a service delivery improvement support through NRW reduction project and hence an AMF of 1.75 was assigned. For the other towns which have no system or not started proper asset management except some reactive responses when problems are encountered, AMF value of 2.0 was assigned.

Based on these adjustment values the WSDLF adjusted ILI values are multiplied by AMF to get the final adjusted ILI value that takes into account both water supply development level and conditions of asset management as indicated in Table 8.

3.1.5 Change in technical performance category

The adjustment of the ILI through the introduction of WSDLF and AMF increased the value of ILI and hence could initiate utilities to improve their water supply system from both perspectives. The last row of Table 8 shows the change in technical performance category.

Town	Addis Ababa	Adama	Mettu	Emdibir	Wolkitae	Debre Markos	Robe	Bedeno	Ginchi
Production (l/c/d)	102.44	59.87	26.17	24.68	28.39	41.20	28.01	28.98	15.47
WSDLF									
(125/Production)	1.22	2.09	4.78	5.06	4.40	3.03	4.46	4.31	8.08
ILI(before adjustment)	9.51	2.97	2.25	1.63	0.64	2.10	0.84	4.09	1.62
ILI _{adj (WSDLF)}	11.60	6.21	10.75	8.27	2.83	6.39	3.76	17.66	13.07
AMF	1.25	1.75	2.00	2.00	2.00	2.00	2.00	2.00	2.00
ILI _{adj(WSDLF_AMF)}									
(after adjustment)	14.50	10.86	21.49	16.55	5.66	12.77	7.52	35.32	26.13
Performance Category									
(before adjustment)	С	А	Α	А	А	А	Α	А	А
Performance Category									
(after adjustment)	С	С	D	D	В	С	В	D	D

Table 8 Determination of ILI adjusted for shortage of water and lack of efficient asset management

All utilities that had performance category of A before adjustment are changed to B, C or D category. Those which moved to category D are the ones with connection of less than 5,000 and where the applicability of the ILI method is in question and are in the urban category IV and V except *Ginchi*. The two towns - *Wolkitae* and Robe - that had a performance category of B were the ones that had ILI of less than 1 which is unrealistic. This is due to higher average pressure and length of main and connection pipe which increased the UARL without a change in CARL. If the initial ILI is changed to one which is theoretically the least and best value of ILI, the adjusted ILI will be 8.80 and 8.92 for *Wolkitae* and *Robe*, respectively which gives a performance category of C for both. Therefore, all the towns had a performance category of poor or very poor that require urgent action to improve the water supply system with respect to real loss which reflects the situation on the ground.

Sensitivity Analysis of Adjustment Factors

The WSDL adjustment factor was varied without changing the AMF to check its sensitivity by decreasing and increasing the per capita water consumption by 25 liters to the minimum and maximum values of 100 and 150 l/c/d. No change in technical performance category was observed in the seven towns. Downgrading to the next technical performance level is observed in Addis Ababa and Robe when the per capita consumption level is above 140 l/c/d. A sensitivity analysis was also carried out by varying the AMF factor from 1.25 to 3.00. No change was observed for Bedeno and Ginchi towns as their initial technical performance was the last one D. With the others change was observed when the AMF is doubled from the minimum to 2.5 and more. In general, the sensitivity analysis showed that both the adjustment factors are robust.

3.2 Discussion

Globally the utilization of the ILI as an index showing utilities performance with regards to real loss management in the last 20 years has shown its effectiveness in a number of cases. However, there were also questions about its applicability in various circumstances. Most of the issues raised were with regards to the reliability of UARL estimate under various circumstances. The main concern was overestimation of UARL due to high pressure in a system leading to lower and misleading ILI values.

In his evaluation of the ILI Wnarni [3], attempted to show that there is no relationship between ILI and NRW expressed as percentage of system input and hence less percentage of NRW does not mean lower ILI. However, it didn't cover the issue of very low water consumption due to different modes of water supply and per capita consumption rates as well as the degree of asset management efforts of utilities. Moreover, the issue of lower ILI values even below 1, UARL being greater than CARL was discussed and attempts were made to develop system correction factor. The expected possible causes that justified the development of correction factors were [23]:

- errors in low CARL volumes derived from Water Balances, or Minimum Night Flows and Night-Day Factors
- errors in infrastructure and/or pressure data inputs to the UARL equation
- lower pressure systems where pressure: leak flow rate relationships are more sensitive than the simplified linear assumption used in the UARL equation
- systems where all bursts surface quickly or are easily and rapidly identified from night flow measurements, including small District Metered Areas.

The adjustments made to address these issues did not consider the effect of the low level of water supply development with respect to prevailing mode of water supply and the lack of proper asset management to decrease leakage in the water utilities of developing countries which are the focus of this paper.

4. CONCLUSIONS

Previous efforts to develop factors could give improved ILIs addressing the issues raised. The author explored other dimensions that contribute for low ILI and recommended adjustment factors to the calculated ILI. This research shows UARL formula is dependent on distribution system parameters and gives similar values whether the system is highly developed with a substantial mode of domestic water supply of house connection or not. The low water consumption levels in developing countries which are mostly based on yard connection implies the quantity of CARL is low. On the other hand, ILI assumes the presence of a systematic asset management with leakage management efforts which is not mostly the case in towns of developing countries. Thus, this paper strongly recommends application of adjustment factors while utilizing the ILI formula in towns of developing countries. The two adjustment factors that consider water supply development level and asset management efforts are developed based on Ethiopian experience and tested. The application of the adjustment factors resulted in higher ILI value that is in line with the extent of the problem. Hence, the author highly recommends the utilization of the formula while investigating urban water supply system of developing countries with similar problems of very low house connections lack of and leakage management system so that the results lead to necessary actions to improve the water supply system and achieve reduction of real water losses.

CONFLICT OF INTEREST

No conflict of interest exists with the author

ACKNOWLEDGMENT

The author would like to thank the water utilities of *Adama, Metu, Emdibir, Wolkitae, Debre Markos, and Ginchi* for providing the basic water distribution system data.

REFERENCES

 Alegre, H., Hirner, W., Melo Baptista, J., Perena, R., "Performance Indicators for Water Supply Services", IWA Manual of Best Practice, 1st Edition. ISBN 90022227, 2000

- [2] Hamilton, S., Mckenzie, R., and Seago, C. "A Review of Performance Indicators for Real Losses from Water Supply Systems", 2005, miya-water.com
- [3] Winarni, W. "Infrastructure Leakage Index (ILI) as Water Losses Indicator", Civil Engineering Dimension, Vol. 11, No. 2, 2009, pp. 126-134.
- [4] Lambert, A.O., "International Report on Water Losses Management and Techniques", Report to IWA Berlin Congress, October 2001. Water Science and Technology: Water Supply vol. 2 no. 4, August 2002.
- [5] Rastegari, E., "How Average Operating Pressure Impacts on Infrastructure Leakage Index", Advances in Ecological and Environmental Research, 2018, 94-103 |Science Signpost Publishing.
- [6] Lambert, A.O., Brown. T. G., Takizawa M., and Weimer, D., "A review of performance indicators for real losses from water supply systems", Journal of Water Supply: Research and Technology-Aqua, vol. 48, no. 6, 1999, pp. 227–237.
- [7] Lambert, A.O. and McKenzie, R.D., "Practical Experience in using the Infrastructure Leakage Index, 'Leakage Management: A Practical Approach", Association International Water Conference in Lemesos, Cyprus in November 2002. Water Board of Lemesos, www.wbl.com.cy
- [8] Alegre, H., Melo Baptista, J., Cabrera, Jr. E., Cubillo, F., Duarte, P., Hirner, W., Merkel, W., Renato Parena, R., "Performance Indicators for Water Supply Services", 3rd Edition, IWA Publishing, 2017.
- [9] Kadu, S. and Dighade, R., "Infrastructure Leakage Index and Challenges in Water Loss Management in Developing Countries", World Environmental and Water Resources Congress: Flood, Droughts and Ecosystems, ASCE, 2015.

- [10] Melaku Abebaw, "Assessment of Water Loss in Water Supply Network, A Case of Debre Markos Town, Regional State of Amhara, Ethiopia", 2015, MSc thesis, School of Civil and Environmental Engineering, Addis Ababa University, Ethiopia.
- [11] Zerihun Abiyu, "Hydraulic Performance Modeling and Improvements of Water Supply Distribution Systems, the Case of Ginchi Town, Regional State of Oromiya, Ethiopia", 2018, M. Sc. thesis, School of Civil and Environmental Engineering, Addis Ababa University, Ethiopia.
- [12] Tegenu Alemayehu and Jemal Mohammed, "Detail Design Report of Bedeno Town Water Supply and Sanitation Project", 2017, Regional State of Oromiya, Ethiopia.
- [13] Addis Ababa Water and Sewerage Authority, "Non-Revenue Water Reduction, Hydraulic Modeling and GIS Development for Addis Ababa City Water Supply System", Water Audit and Benchmarking Report, 2012, Ethiopia
- [14] Majer Behute, "Assessment of Wolkite Water Supply System in Gurage Zone, SNNPR, Ethiopia, School of Civil and Environmental Engineering", 2016, M. Sc. thesis, Addis Ababa University, Ethiopia.
- [15] Biniyam Bogale, "Assessment of the Water Distribution Network of Metu Town Water Supply System, Regional State of Oromiya, Ethiopia",2016, MSc thesis, School of Civil and Environmental Engineering, Addis Ababa University, Ethiopia.
- [16] Dereje Wakjira, "Performance Evaluation of Distribution System, Case Study of Adama Town, Regional State of Oromiya, Ethiopia", 2014, M. Sc. thesis, School of Civil and Environmental Engineering, Addis Ababa University, Ethiopia.

- [17] Antoniyos Wodajo, "Assessment of Emdibir Town Water Supply System, Cheha Woreda, Gurage Zone, SNNPR, Ethiopia", 2017, M. Sc. thesis, School of Civil and Environmental Engineering, Addis Ababa University, Ethiopia.
- [18] Liemberger, R. and Brothers, K., Lambert, A., McKenzie, R., Rizzo A., and Waldron, T. "Water Loss Performance Indicators", Water Loss Conference, 1, 2007, pp. 148-160, Bucharest, Romania.
- [19] Federal Democratic Republic of Ethiopia, National Planning Commission.
 "Growth and Transformation Plan II (GTP II) (2015/16 – 2019/20) Volume I: Main Text", National Planning Commission, 2016, Ethiopia.
- [20] Addis Ababa Water and Sewerage Authority, "Addis Ababa Water Distribution and Operation Management and Hydraulic Modelling Report", 2019, Ethiopia.
- [21] Liemberger R. and Mc Kenzie.,
 "Accuracy Limitations of the ILI Is it an Appropriate Indicator for Developing Countries?", 2005, Leakage 2005 -Conference Proceedings, D Pearson, SW Trow - rash.apanela.com.
- [22] Yoseph Kebede, Geremew Sahilu, Kefyalew Muleta and Tesfaye Adnew., "Technical and Social Factors affecting service quality of water utilities in small and medium towns, the case of East Shewa zone of Oromia", 2019, Ethiopia, Ethiopian Water Technology Institute, Ministry of Water and Energy, Ethiopia.
- [23] Lambert, A. O., "System Correction Factor SCF can customize the standard UARL equation for pipe materials, small systems and pressure: bursts relationships", 2020, Leakssuite Library Ltd.