

MODELLING AND ANALYSIS OF HEAT TRANSFER MECHANISM OF A SOLAR HEATER COVER AND ABSORBER PLATE

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Abstract

The analysis and the process by which heat transfer occurs between a solar heater cover and absorber plate as well as the analysis of radiative heat transfer mechanism are presented. The fluid motion is due to forced convection. Experimental and theoretical studies on the system's performance are also presented. The heated water temperature T_w is recorded in the range 75°C - 79°C in December, 2003 and in the range of 81°C - 84°C in January, 2004. The peak temperature in each case was between 1200hrs and 1400hrs with a peak value at 1300hrs. The systems radiative heat mechanism was found to be highly good. The result of the analysis of heat transfer mechanism of a solar heater cover together with the absorber plate show that it is very effective for domestic use. The result shows that the system remains very effective hence delivers heated water up to a maximum temperature of 84°C .

Keywords: Solar heater cover, absorber plate, energy storage, food processing
And solar radiation.

1. Introduction

Technical advances in solar water heating have been very rapid in the last 40 years. It has been of obvious benefits to house holders especially in those areas where the climate is ideally suited for the application of solar energy for water heating, particularly in the present situation of acute energy shortage. Solar water heaters find wide applications in large establishments such as hospitals, hotels, students

hostels, industries including food processing, paper and textile, domestic uses and in heating swimming pools. The temperature requirement can easily be achieved with simple equipment, Garg and Prakash (2002). It is always advisable to use flat-plate collectors instead of concentrators in the development work. In the past years, almost all solar water heaters are based on the principle of flat-plate

collector. Most pioneering work have been widely spread all over the world, including Europe, America, Asia, Caribbean and Africa.

The main objective of the experiment is to convert as much solar radiation as possible into heat at the highest attainable temperature and for the lowest possible investment in materials and labour.

Glass is an interesting cover material for solar thermal devices due to its ability to absorb almost all the infrared (IR) radiation re-emitted by the absorber plate. In effect it succeeds in creating a green house effect which enhances the thermal efficiency of the solar collector. This has been confirmed by Jannot and Coulibally (1997). The use of glass as a solar collector cover has two major disadvantages; the high cost Njomo (1995), and its fragile nature during its transportation and in service. Transparent plastic covers (especially polyethylene) are used widely in developing countries in the rural areas because they are always available and

can be used to construct moderate cost solar air heaters. Charters et al, (1989) and GRET (1986), have stated that these collectors are used mainly for foodstuff drying. The transmissivity of polyethylene to infrared radiation is $T_a = 0.82$, Classen and Buttler (1980). The measurement of some temperature characteristics such as ambient, T_a , chamber, T_c and water, T_w , of a solar water heater in addition to the average total solar radiation in $\text{mJm}^2 \text{d}$ were taken for Awka, Nigeria. In this paper, the radiative equations of the absorber plate, the transparent cover and heat transfer mechanism are examined. Malhortra et al (1981) stated that the glass and plastic materials of interest have refractive indices of 1.5.

2. Experimentation

Two different experiments were carried out on two different periods, December 10, 2003 and January 17, 2004 and ambient, T_a , chamber, T_c and water, T_w temperatures, determined. The results are shown in Table 1 for 10 hours starting from 0800 hours to 1800 hours. Another experiment was carried out

Table 1: Ambient temperature, T_a , chamber temperature, T_c , and water temperature, T_w , of a solar water heater measured on December 10, 2003 and January 17, 2004.

Time in hrs	December 10, 2003			January 17, 2004		
	T_a °C	T_c °C	T_w °C	T_a °C	T_c °C	T_w °C
0800	27	34	37	28	35	41
0900	28	45	50	29	48	55
1000	29	50	65	30	55	67
1100	31	61	73	32	62	75
1200	33	65	80	34	68	81
1300	35	76	83	36	79	84
1400	38	73	77	39	75	80
1500	35	70	74	37	72	78
1600	32	67	70	33	68	75
1700	29	62	66	31	64	71
1800	28	59	62	28	61	65

the means of the monthly maximum water temperature reached in the solar heater determined, the ambient temperature T_a as well as the temperature of the system, (absorber) T_s and the total radiation H_0 on horizontal surface at Awka, Nigeria, (6.12°N, 7.05°E) were also determined. The means of the monthly maximum, proposed by Klein, (1977) was used. In

the proposal, Klein suggested using d_n for the mean day of the month, hence the equivalent n to be used is shown in Table 2, and in equation (1) for the year 2004. The Linke Feussner pyrheliometer was used to measure the monthly average of the total solar radiation H_0 in $\text{mJ}/\text{m}^2\text{d}$ for January 17, 2004. The results are recorded in Table 2.

Table 2: Monthly mean solar radiation parameters and the mean of maximum ambient temperature, T_a , and system temperature, T_s , of a solar water heater measured in 2004.

Monthly average, d_n	N	Declination δ	Hour angle w°	Hour angle radian	$T_a, ^\circ\text{C}$	$T_s, ^\circ\text{C}$	Average Total Solar radiation H_0 in $\text{MJ}/\text{M}^2\text{-d}$	ϵ_0
Jan. 17	17	-20.92	87.65	1.533	37	77	43.02	1.0300
Feb. 16	47	-12.95	88.59	1.546	35	75	43.00	1.0251
Mar. 16	75	-2.42	74.96	1.308	33	71	39.11	1.0108
April 15	105	9.41	91.02	1.589	31	69	34.98	0.9938
May. 15	135	18.79	92.09	1.607	30	66	28.99	0.9780
June 11	162	23.09	92.49	1.614	30	64	25.47	0.9692
July. 17	198	21.18	92.38	1.613	29	63	25.33	0.9674
Aug. 16	228	13.45	91.47	1.597	31	65	28.98	0.9746
Sept. 15	258	2.22	90.24	1.575	31	67	34.27	0.9885
Oct. 15	288	-9.60	88.96	1.553	32	70	38.68	1.0058
Nov. 14	318	-18.91	87.89	1.534	33	73	40.94	1.0222
Dec. 10	344	-23.05	87.39	1.525	34	75	41.83	1.0319

The eccentricity correction factor ϵ_0 , equivalent for the average days are recorded and given from a more detailed expression, (Duffie and Beckman, 1991).

Theory

Garg and Prakash (2002) had proposed that for the average total solar radiation, the appropriate equation is given by

$$H_0 = \frac{24}{\pi} I_{sc} (1 + 0.33 \cos \frac{360n}{365}) \times$$

$(\cos \Phi \cos \delta \sin \omega + \omega \sin \Phi \sin \delta)$ (1)
 where I_{sc} is the equivalent solar constant given by $4921 \text{ kJ/m}^2\text{hr}$ and δ is the sun's declination Cooper (1969), has given the sun's declination equation as

$$\delta = 23.45 \sin \left\{ \frac{360(284 + dn)}{365} \right\} \quad (2)$$

3. Performance Prediction of Solar Water Heater

Zallner *et al.* (1985) stated that thermal optimization of built-in-storage water heater must be based on the evaluation of system performance under diverse conditions. The instantaneous heat balance as illustrated in Fig. 1 according to Garg (1975), may be written in the form: radiation absorbed = heat absorbed by water + heat absorbed by container + heat loss from the absorber. It is assumed that for practical purposes (under steady state conditions) that the water temperature is equal to the absorber temperature, hence $T_w = T_c$ and

$$\frac{dT_w}{dt} = \frac{dT_c}{dt} \quad (4)$$

Equation (4) thus becomes

$$X \frac{dT_w}{dt} + Y T_w = Z \quad (5)$$

where $X = W_w + W_c +$

$$(U_L + U_B) A_c / 2 \quad (6)$$

$$Y = (U_L + U_B) A_c \quad (7)$$

$$Z = I T_i (T_a) A_c + (U_L +$$

$$U_B) \frac{A_c}{2} \left[\frac{dT_a}{dt} + 2T_a \right] \quad (8)$$

The solution to eqn. (5) is

$$T_w = \frac{Z}{Y} + (T_{wi} - \frac{Z}{Y}) \exp \left[\frac{-Y}{X} (t - t_i) \right] \quad (9)$$

where T_{wi} is the initial water temperature at time t_i , when fresh water is added.

The radiative heat transfer equation hr_1 from plate to cover were shown by Sukhame (1984), Williams (1983),

with hour angle as

$$\omega = \cos^{-1} (-\tan \Phi \tan \delta) \quad (3)$$

where Φ is the latitude location of the place.

Garg (1982) as well as by Whillier and Saluja (1964) as

$$hr_1 = \frac{\bar{\sigma} T_p^2 + T_1^2 (T_p + T_1)}{(1/\epsilon_p + 1/\epsilon_1 - 1)} \quad (10)$$

where $\bar{\sigma}$ is Stefan - Boltzmann's constant, T_p is the temperature of the plate, T_1 is the cover temperature, ϵ_p is the emissivity of the plate and ϵ_1 is the cover emissivity respectively. Also the radiative heat loss from plate to cover is given by

$$Hr_p = \frac{\bar{\sigma} T_p^2 + T_1^2 (T_p + T_1)}{(1/\epsilon_p + 1/\epsilon_1 - 1)} \quad (11)$$

It is also noted that if the depth or distance between upper and lower plates of the system increases, the collector efficiency increases since the thermal losses to the outside air decreases.

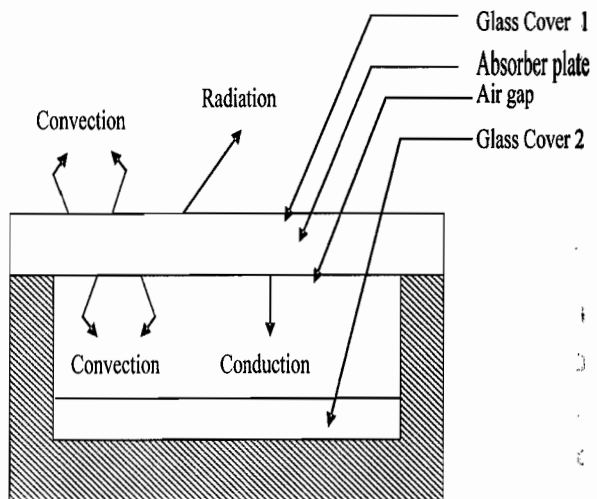


Fig. 1: Illustration of built-in-storage type solar water heater.

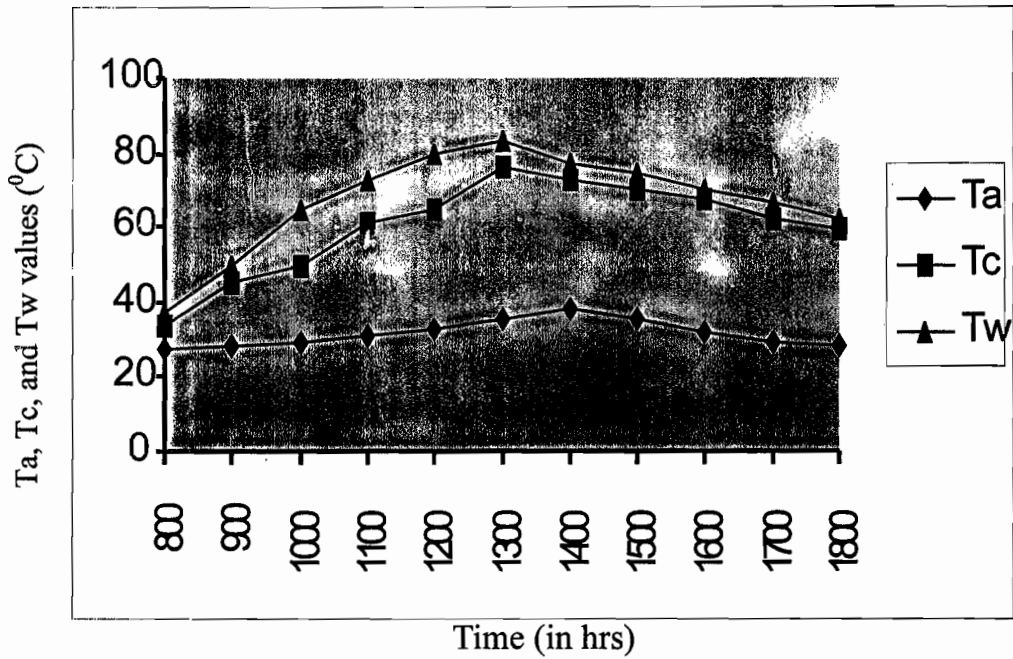


Fig. 2: Hourly variation of ambient temperature T_a , chamber temperature T_c , and water temperature T_w of a solar water heater on December 10, 2003.

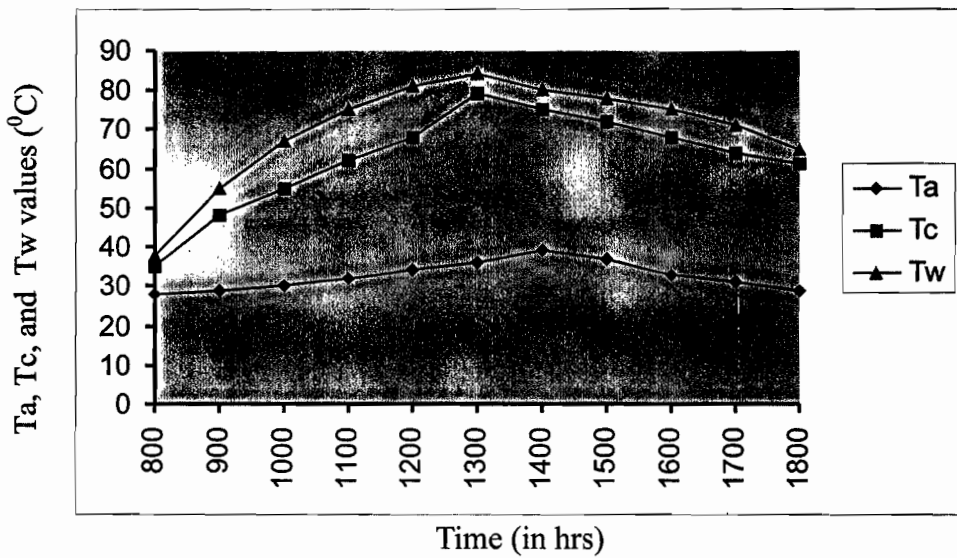


Fig. 3: Hourly variation of ambient temperature T_a , chamber temperature T_c , and water temperature, T_w of a solar water heater on January 17, 2004.

4. Results and Discussion

Results show that the monthly average of the daily maximum temperature of the water in the solar heater lies in the range 71°C - 77°C in the month of January to March 2004 and in the range 70°C - 75°C from October to December of the same year, Table 2.

In Table 1, various values of ambient temperature T_a , collector temperature T_c , and water temperature T_w show that the temperatures were in steady rise until it attained maximum at 1300 hours after which the values steadily decreased as the sun's declination disappear. A maximum temperature of 84°C was attained for the system. In Table 2, the various measured values of average total solar radiation in $\text{mJ}/\text{m}^2\text{d}$ are shown. Maximum and minimum values were attained in the month of January, 2004. This gradually decrease started rising again steadily in the

month of October. The systems temperatures were also found to be high in the months with high average total solar radiation and at the same time low in the months with low average total solar radiation. The graphical illustration in Figs. 2 and 3 each show the variation of the measured ambient temperature T_a , chamber temperature T_c and water temperature T_w for December 2003 and January, 2004 respectively. The peak temperature in each case was between 1200hrs and 1400hrs with the peak value at 1300hrs. The ambient temperature T_a in each case was found to be lowest. It was also observed that while Fig. 4 shows the monthly average of the daily maximum of the measured ambient temperature T_a and system temperature T_s , Fig. 5 shows the variation of the monthly average total solar radiation H_o for 2004.

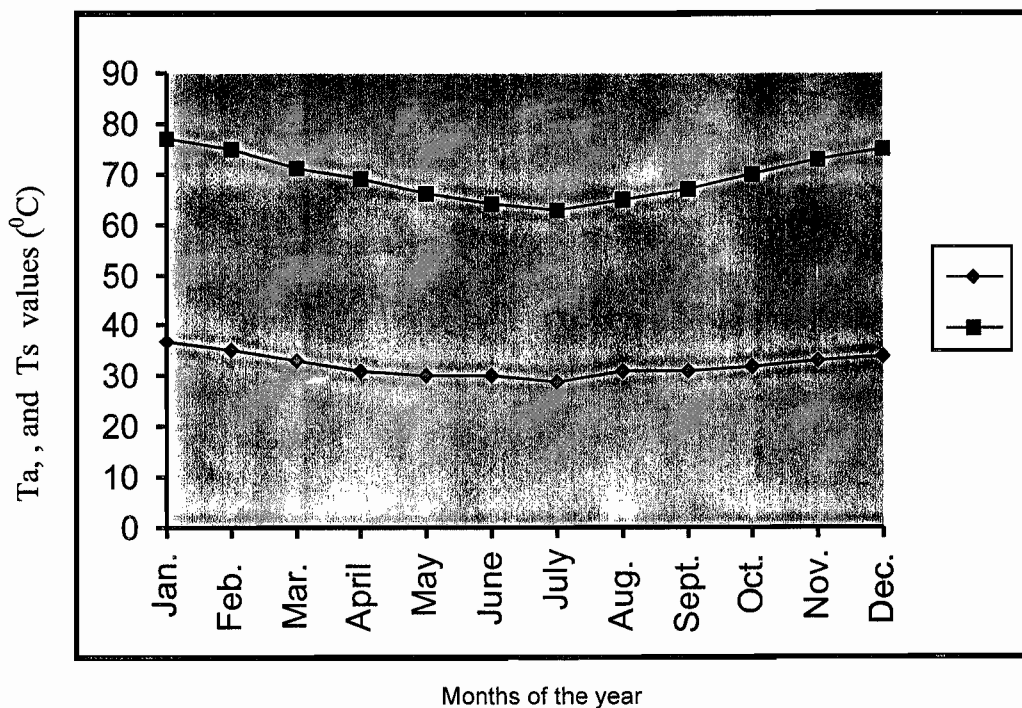


Fig. 4: Monthly average of the daily maximum of ambient temperature, T_a , and systems (absorber) temperature, T_s , of a solar water heater measured in 2004.

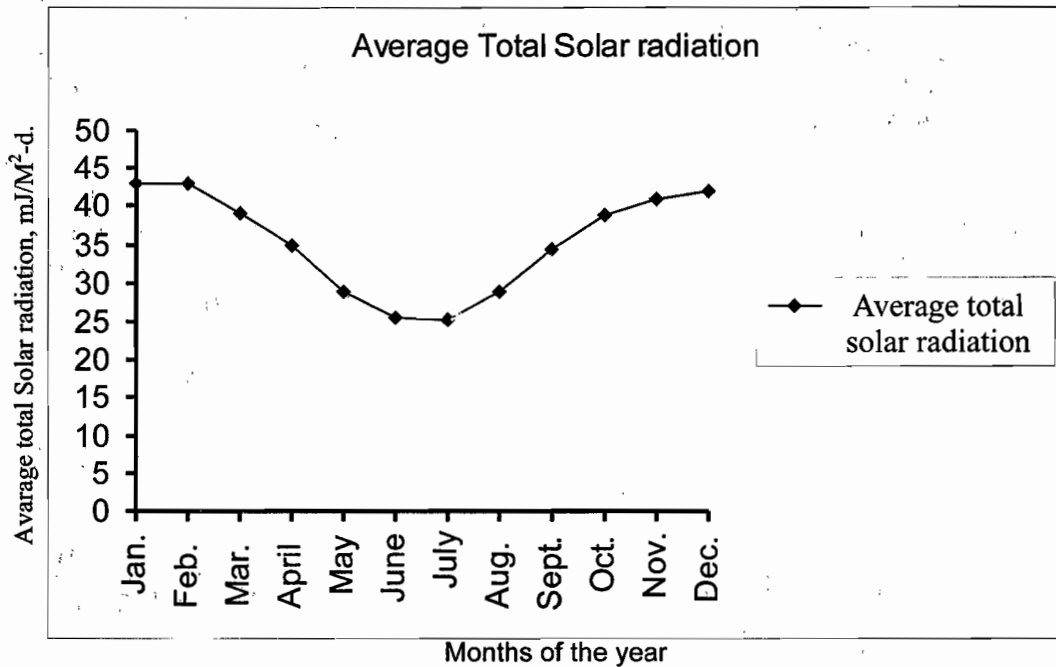


Fig. 5: Variation of monthly average total solar radiation H_0 for 2004.

5. Conclusion

The systems radiative heat mechanism was found to be highly good. The results show that hot water temperature varied from 71°C to 77°C in the months of January to March, 2004 and 70°C to 75°C in the months of October to December of the same year. The results are confirmed to be in line with that of Garg and Prakash (2002). The result of the analysis of heat transfer mechanism of a solar heater cover together with the absorber plate has supported the use of solar energy for domestic purposes. The results of the average total solar radiation H_0 obtained in the experiment was in line with that obtained by Garg (1975) and Zallner *et al.* (1985).

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