

# EFFECTS OF LITHOLOGY ON GEOTHERMAL GRADIENT IN THE SOUTH-EAST NIGER DELTA, NIGERIA

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## ABSTRACT

A study of the effects of lithologic formations on geothermal gradients is carried out in the south-east Niger Delta, Nigeria, using continuous temperature and lithologic log data from closely-spaced petroleum wells. The gradient profiles obtained for the deep wells, logged to depths between 6500 ft (1981m) and 8500ft (2591m), were observed to have markedly different geothermal gradients with corresponding vertical lithologic units. For the upper sandy lithology, the Benin Formation, the temperature gradient ranges between 0.80 °F/100 ft (1.456 °C/100m) and 1.22 °F/100 ft (2.220 °C/100m) with an average of 1.03 °F/100 ft (1.875 °C/100m). For the paralic shaly Agbada Formation segment, the temperature gradient ranges between 0.92 °F/100 ft (1.674 °C/100m) and 1.87 °F/100ft (3.403 °C/100m) with an average of 1.40 °F/100ft (2.548 °C/100m). The depths of Benin Formation were observed to vary between 4200ft (1280 m) and 5400ft (1879 m). Geothermal gradients are thus observed to increase with depth and shale units.

**Key Words:** Subsurface temperature, lithology, temperature gradient, thermal conductivity, basin, fluid flow.

## INTRODUCTION

We examine here the geothermal field of the south-east Niger Delta using continuous well-log temperature data from closely-spaced 4 wells. The study area covers the geographical grids of 7°15' – 7°40'E and 4°24' – 5°43'N (Figure 1). In this study temperature was digitized every 100 feet from petroleum exploratory well logs, which were furnished by The Shell Petroleum Development Company of Nigeria Limited. These data are confidential hence the names of the wells are coded. Many researchers have highlighted the importance of using well-log temperature for geothermal investigations (Moses, 1961; Anglin and Beck, 1965; Schoepel and Gilarranz, 1966; Harper, 1971; Connolly, 1972; Uko, 1996; and Akpabio, 1998).

Knowledge of sub-surface temperature distribution is useful in understanding the mechanism of basin formation and geological processes such as rifting, and the development of major volcanic fields (Reiter and Jessop, 1985). Temperature data from wells logged to total depth in the Niger delta could be used to derive estimates of regional temperatures and geothermal gradients in the area (Nwachukwu, 1976). Temperature data is an important parameter in the investigations of hydrocarbon maturation (Tissot and Welte, 1978; Waples, 1980; Ungerer, 1984). Representations of heat flow data in contour maps offer suggestions for

the interpretations of crustal tectonics and large-scale hydrodynamics, and formation of basins (Lachenbruch and Sass, 1977; Blackwell, 1978; Royden *et al.*, 1980; Majorowicz, *et al.*, 1986).

Knowledge of subsurface temperature profile cannot be overemphasized in the bid to understanding the geologic as well as geophysical processes in any given sedimentary basin such as the Niger Delta.

Furthermore, knowledge of borehole temperature and geothermal gradients is necessary for the analysis of reservoir fluid properties, as well as plate tectonic interpretation, heat flow and geothermal energy utilization (Reike, 1974; Avbovbo, 1978; Moses, 1961). Temperature is one of the primary factors controlling hydrocarbon generation, sediment diagenesis and migration of hydrocarbons and other pore fluids (Ejedawe, 1981; Avbovbo, 1978; Beck, 1965; Uko, 1996).

The main aim of this paper is to investigate the relationship between geothermal gradient and lithology in the south-east Niger Delta, Nigeria.

## REGIONAL GEOLOGY

The Niger Delta situated at the West African margin of the Gulf of Guinea, is a large arcuate delta, which occupies an area located between longitude 4° – 9°E and latitudes 4° – 6°N (Figure 2). The geology of Niger Delta has been

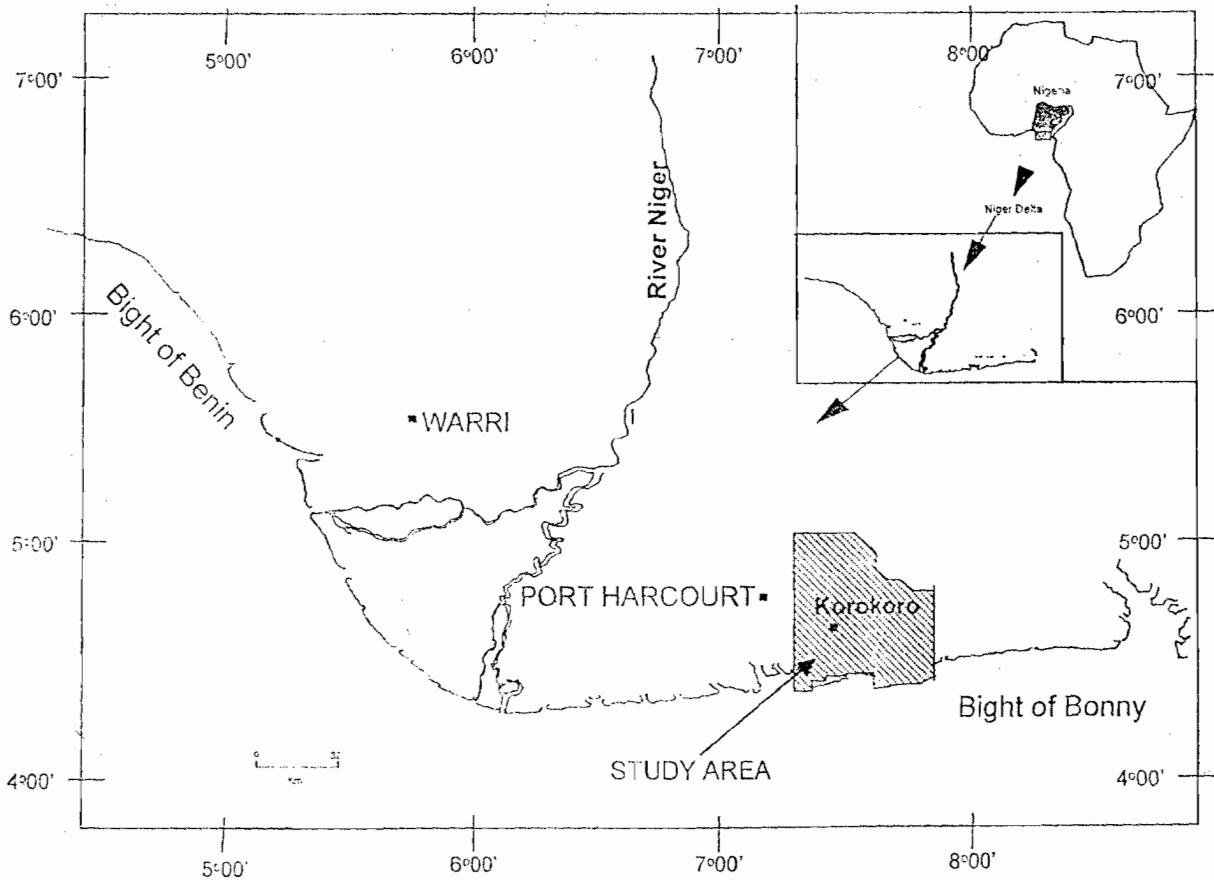


Fig. 1: Southern Nigeria showing the Niger Delta region and the study area

described by many investigators (Hospers, 1965; Short and Stauble, 1967; Murat, 1970; Weber, 1971; Ofoegbu, 1985; Uko *et al.*, 1992). Sediment deposition in the southern Niger delta was controlled by three main tectonic phases. The first tectonic cycle in the Albian resulted in the formation of the Benue and Abakaliki troughs and the in-filling by Albian shales and sandstones. This period also marked the establishment of the Calabar and Benin flanks. The second tectonic cycle was marked by the folding of sediments during the Santonian. This episode was followed by considerable magmatic activity and mineralization. The third cycle, the late Eocene, led to the establishment of the modern Niger delta (Assez, 1989; Novelli, 1974), Figure 3. Growth faulting occurred in parallel with the coast, contemporaneous with progradation, and sedimentation. Three major sedimentary formations make up the present day Niger Delta. These are the Benin, Agbada, and the Akata Formations.

The Benin Formation is the alluvial or upper coastal plain depositional environment of

the Niger Delta Complex. It extends from the west Niger Delta across the entire Niger Delta area and to the south beyond the present coastline. The Benin Formation consists of coarse-grained, garvelly sandstone with minor intercalation of shale. It is a continental deposit of Miocene to younger in age and has a thickness in excess of 1820m. Typical outcrops of the Benin Formation can be seen around Benin, Onitsha and Owerri (Figure 3).

The Agbada Formation underlies the Benin Formation. It was laid down in parallel brackish to marine fluvial, coastal environments. The Agbada Formation is made up primarily of alternating sandstones and shales and is of fluvio-marine origin. It ranges in age from Eocene in the north to Pliocene in the south. These sands, sandstones, and marine shales, which make up the Agbada Formation, attain a maximum thickness of about 4500m. The Agbada Formation is time equivalent to the Ogwashi-Asaba-Ameki Formation further north.

The Akata Formation is the lowest unit of the Niger Delta Complex. It was deposited in a

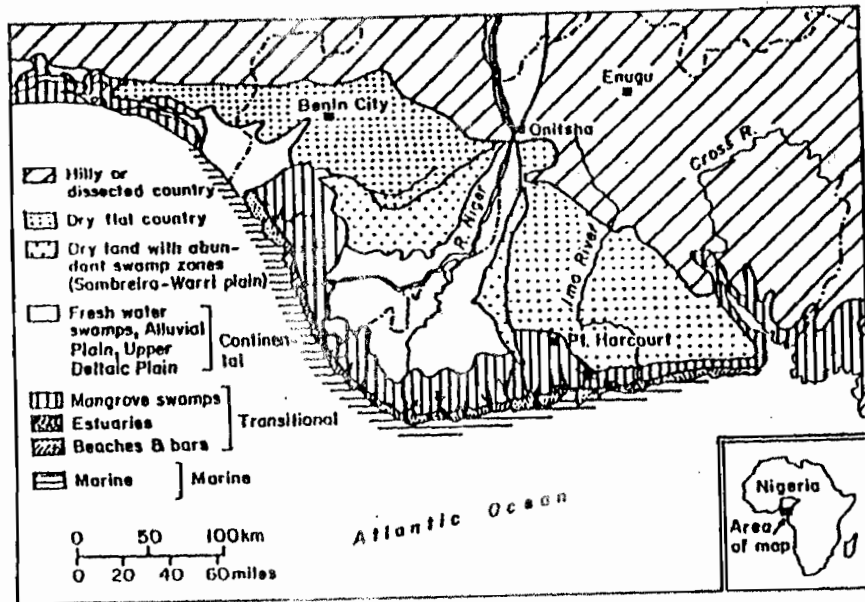


Fig. 2: Geological features and sedimentary environment of the Niger Delta (After Short and Stauble, 1967)

typical marine environment. The Akata Formation, on the other hand, consists of shales with local interbedding of sands and siltstones. The Formation becomes shalier with depth. It was deposited in a marine environment and the Formation outcrops offshore in shale diapirs (Weber, 1971; Mascle *et al.*, 1973). The thickness of Akata Formation may reach 7000 m in the central part of the delta. The Akata Formation ranges from Eocene to Recent (Hospers, 1965; Short and Stauble, 1967; Kogbe, 1976; Ofoegbu, 1985).

#### DATA ACQUISITION AND ANALYSIS

Data consisted temperatures digitized from continuous temperature logs from four closely-spaced oil wells, which were drilled between 1960 and 1962. The logs were supplied by The Shell Petroleum Development Company of Nigeria. The continuous temperature data, which were of good quality and logged to depths of 6500, 7200, 7200, and 8500 feet, were available at different depths, allowing the calculation of an average temperature gradient. The continuous temperature data allow a high confidence level to be attached to the results. Temperature corrections for drilling mud circulation effect (Chapman *et al.*, 1984) require multiple bottom-hole-temperature measurements at various times and depths in order to extrapolate to the actual temperature of formations (Dowdle *et al.*, 1975). It was not possible to correct the temperatures because the

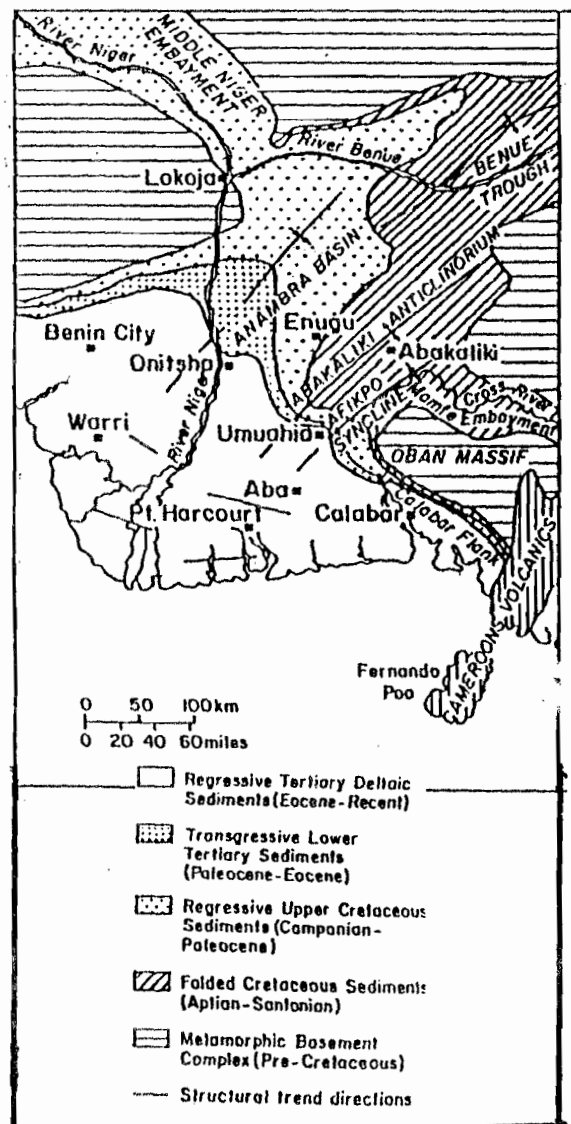


Fig. 3: Structural features of the southern Nigerian basin (After Short and Stauble, 1967)

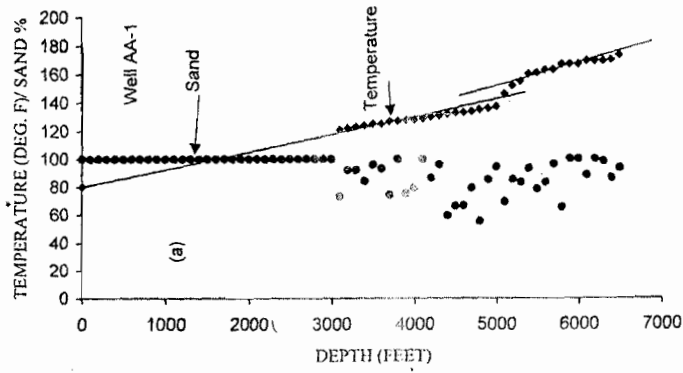


Fig. 4a: Depth-Temp/Sand % Profile for Well AA-1

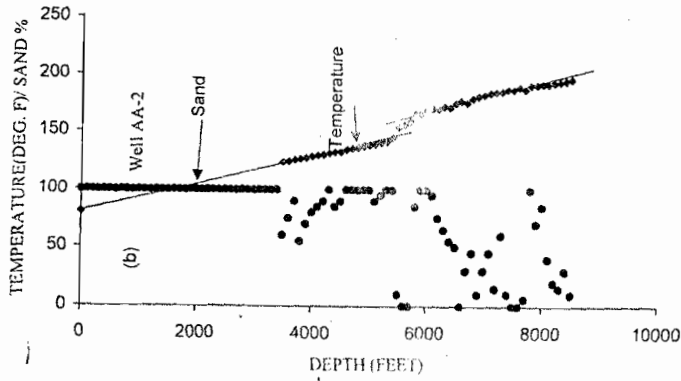


Fig. 4b: Depth-Temperature/Sand % Profile for Well AA-2

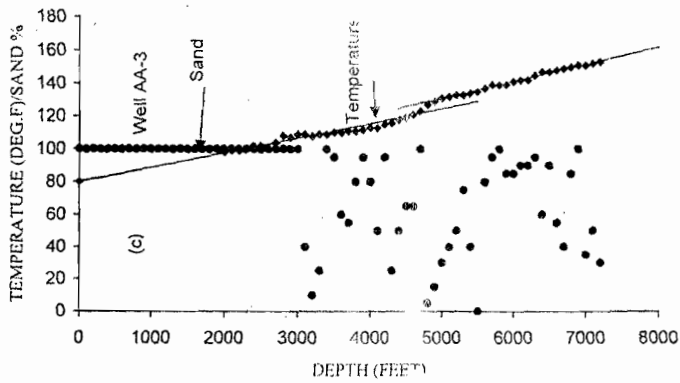


Fig. 4c: Depth/Temperature-Snad % Profile for Well AA-3

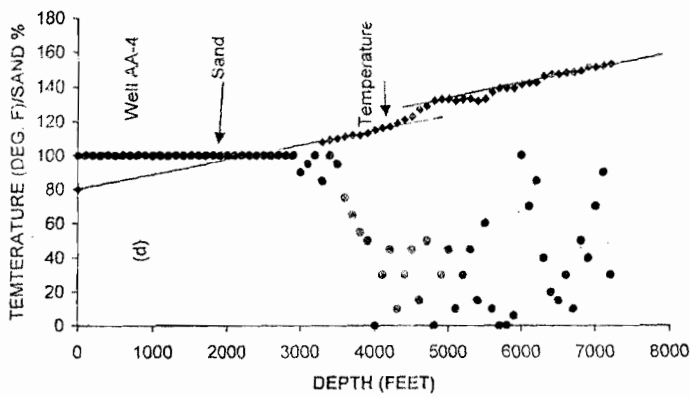


Fig. 4d: Depth-Temperature/Sand % profile for Well AA-4

Fig. 4: Depth-temperature/Sand % profiles for Wells AA-1, AA-2, AA-3 and AA-4

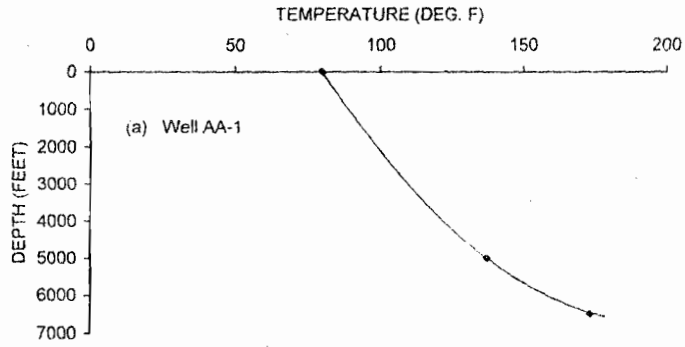


Fig. 5a: Depth-temperature curve based on 2 bottom-hole-temperatures measured at Total Depth (DT) for Well AA-1

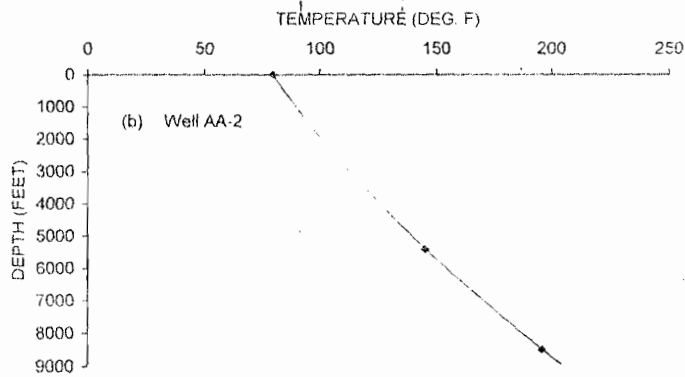


Fig. 5b: Depth-temperature curve based on 2 bottom-hole-temperatures measured at Total Depth (DT) for Well AA-2

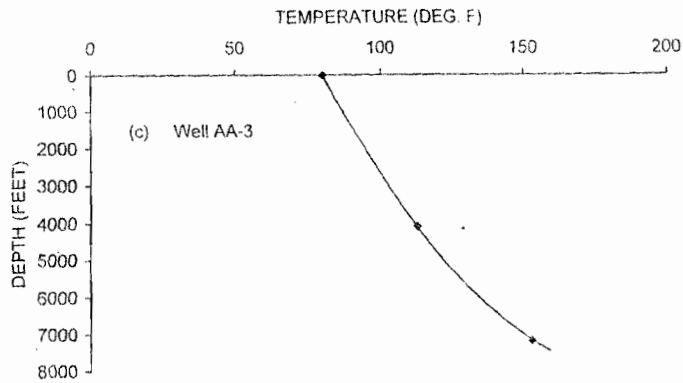


Fig. 5c: Depth-temperature curve based on 2 bottom-hole-temperatures measured at Total Depth (TD) for Well AA-3

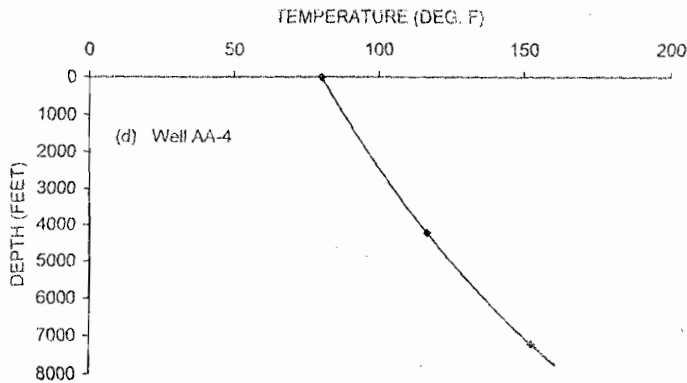


Fig. 5d: Depth-temperature curve based on 2 bottom-hole-temperatures measured at Total Depth (TD) for Well AA-4

Fig. 5: Depth-temperature curves based on 2 bottom-hole-temperatures measured at Total Depth (TD) for Wells AA-1, AA-2, AA-3 and AA-4

TABLE 1: Temperature, Sand percentage with depth for the Wells

(a) Well AA-1

| Depth<br>(ft) | Temperature<br>(°F) | Sand<br>(%) |
|---------------|---------------------|-------------|
| 0             | 80                  | 100         |
| 0 - 3000      | -                   | 100         |
| 3100          | 121                 | 73          |
| 3200          | 122                 | 92          |
| 3300          | 123                 | 92          |
| 3400          | 124                 | 84          |
| 3500          | 125                 | 96          |
| 3600          | 125                 | 93          |
| 3700          | 127                 | 74          |
| 3800          | 127                 | 100         |
| 3900          | 128                 | 75          |
| 4000          | 128                 | 79          |
| 4100          | 129                 | 100         |
| 4200          | 130                 | 86          |
| 4300          | 131                 | 96          |
| 4400          | 132                 | 59          |
| 4500          | 133                 | 66          |
| 4600          | 133                 | 66          |
| 4700          | 134                 | 79          |
| 4800          | 135                 | 55          |
| 4900          | 136                 | 85          |
| 5000          | 137                 | 94          |
| 5100          | 146                 | 69          |
| 5200          | 152                 | 85          |
| 5300          | 155                 | 83          |
| 5400          | 160                 | 93          |
| 5500          | 161                 | 78          |
| 5600          | 163                 | 83          |
| 5700          | 163                 | 96          |
| 5800          | 167                 | 65          |
| 5900          | 167                 | 100         |
| 6000          | 167                 | 100         |
| 6100          | 169                 | 88          |
| 6200          | 169                 | 100         |
| 6300          | 169                 | 98          |
| 6400          | 170                 | 86          |
| 6500          | 173                 | 93          |

logs lacked the required header information on circulation time, and time elapsed since circulation. The equilibrium temperature of the formations was therefore estimated by a factor of 10% increment (Chukwueke *et al.*, 1992 and Akpabio, 1998). However, Akpabio (1998) has stated that temperature data used in evaluating the temperature variation in the Niger Delta from well logs have duration of well stabilization of 30 days and above, a period from well completion to logging in which the well has attained equilibrium or near equilibrium. Since there was no header information, we do not know whether the wells met the 30-day duration. A surface temperature of 27°C (80°F) has been assumed for the Niger Delta.

For the temperature logs, downhole temperature values are read off, at 100ft intervals, directly from the logs. The formation sand-shale lithology was obtained from the Gamma Ray logs from which sand percentages were also obtained at 100ft-interval. The temperatures and sand percentages with depths are given in Table 1. The temperatures were plotted against depth and sand percentage. Figure 4 gives the temperature gradients, and lithology profiles for the four wells. The data points were then divided into defined segments. Each segment is fitted to a straight line whose slope represents the temperature gradient within the lithology. The lithologic temperature gradient was computed separately for each lithology using equation (1). Then the average of

(b) Well AA-2

| Depth (ft) | Temperature (°F) | Sand (%) | Depth (ft) | Temperature (°F) | Sand (%) |
|------------|------------------|----------|------------|------------------|----------|
| 0          | 80               | 100      | 7000       | 182              | 30       |
| 0 - 3400   | -                | 100      | 7100       | 184              | 45       |
| 3500       | 124              | 60       | 7200       | 185              | 15       |
| 3600       | 125              | 75       | 7300       | 185              | 60       |
| 3700       | 126              | 90       | 7400       | 187              | 10       |
| 3800       | 127              | 55       | 7500       | 187              | 0        |
| 3900       | 128              | 70       | 7600       | 189              | 0        |
| 4000       | 129              | 80       | 7700       | 187              | 6        |
| 4100       | 130              | 85       | 7800       | 191              | 100      |
| 4200       | 131              | 90       | 7900       | 191              | 70       |
| 4300       | 132              | 100      | 8000       | 192              | 85       |
| 4400       | 133              | 85       | 8100       | 192              | 40       |
| 4500       | 133              | 90       | 8200       | 193              | 20       |
| 4600       | 135              | 100      | 8300       | 194              | 15       |
| 4700       | 136              | 100      | 8400       | 195              | 30       |
| 4800       | 137              | 100      | 8500       | 196              | 10       |
| 4900       | 138              | 100      |            |                  |          |
| 5000       | 139              | 100      |            |                  |          |
| 5100       | 140              | 90       |            |                  |          |
| 5200       | 141              | 95       |            |                  |          |
| 5300       | 142              | 100      |            |                  |          |
| 5400       | 145              | 100      |            |                  |          |
| 5500       | 154              | 10       |            |                  |          |
| 5600       | 156              | 0        |            |                  |          |
| 5700       | 159              | 0        |            |                  |          |
| 5800       | 165              | 85       |            |                  |          |
| 5900       | 166              | 100      |            |                  |          |
| 6000       | 169              | 100      |            |                  |          |
| 6100       | 170              | 95       |            |                  |          |
| 6200       | 170              | 75       |            |                  |          |
| 6300       | 172              | 65       |            |                  |          |
| 6400       | 171              | 55       |            |                  |          |
| 6500       | 175              | 50       |            |                  |          |
| 6600       | 177              | 0        |            |                  |          |
| 6700       | 175              | 30       |            |                  |          |
| 6800       | 179              | 45       |            |                  |          |
| 6900       | 181              | 10       |            |                  |          |

was calculated and used for the interpretations.

Several and relative methods exist for the determination of geothermal gradients (Nwachukwu 1976, Basssiouni, 1994; Avbovbo, 1978; Speece *et al.*, 1985 and Uko, 1996). Speece *et al.* (1985) have documented the method of formation and lithology, temperature gradient by the least square method. The least-squares lithology temperature gradients are used to estimate temperature gradients for each formation on the basis of the lithological make up of each formation encountered in a borehole. In a vertical borehole penetrating a horizontally layered sequence of formations the geothermal gradients in a formation in a given borehole are calculated using the equation,

$$\left(\frac{dT}{dz}\right)_f = \sum_{i=1}^n \left[ \left(\frac{dT}{dz}\right)_i \frac{h_i}{d} \right]$$

where  $(dT/dz)_f$  is the temperature gradient of the formation being considered, derived lithologically,  $(dT/dz)_i$  is the temperature gradient of the *i*th lithology within the formation and  $h_i$  is the thickness of the *i*th lithology and  $d$  is the formation thickness.

From the temperature-depth profiles, the geothermal gradients, so obtained, show an increase of gradient with more shale units. Owing to the few wells, we could not obtain isothermal contour map for the area.

(c) Well AA-3

| Depth (ft) | Temperature (°F) | Sand (%) | Depth (ft) | Temperature (°F) | Sand (%) |
|------------|------------------|----------|------------|------------------|----------|
| 0          | 80               | 100      | 5600       | 137              | 80       |
| 0 - 1900   | -                | 100      | 5700       | 139              | 95       |
| 2000       | 98               | 100      | 5800       | 139              | 100      |
| 2100       | 99               | 100      | 5900       | 139              | 85       |
| 2200       | 99               | 100      | 6000       | 141              | 85       |
| 2300       | 100              | 100      | 6100       | 142              | 90       |
| 2400       | 102              | 100      | 6200       | 142              | 90       |
| 2500       | 102              | 100      | 6300       | 145              | 95       |
| 2600       | 100              | 100      | 6400       | 147              | 60       |
| 2700       | 104              | 100      | 6500       | 147              | 90       |
| 2800       | 108              | 100      | 6600       | 148              | 55       |
| 2900       | 107              | 100      | 6700       | 149              | 40       |
| 3000       | 109              | 100      | 6800       | 150              | 85       |
| 3100       | 109              | 40       | 6900       | 151              | 100      |
| 3200       | 108              | 10       | 7000       | 151              | 35       |
| 3300       | 109              | 25       | 7100       | 152              | 50       |
| 3400       | 109              | 100      | 7200       | 153              | 30       |
| 3500       | 110              | 95       |            |                  |          |
| 3600       | 110              | 60       |            |                  |          |
| 3700       | 111              | 55       |            |                  |          |
| 3800       | 111              | 80       |            |                  |          |
| 3900       | 112              | 95       |            |                  |          |
| 4000       | 113              | 80       |            |                  |          |
| 4100       | 113              | 50       |            |                  |          |
| 4200       | 115              | 95       |            |                  |          |
| 4300       | 116              | 25       |            |                  |          |
| 4400       | 118              | 50       |            |                  |          |
| 4500       | 119              | 65       |            |                  |          |
| 4600       | 121              | 65       |            |                  |          |
| 4700       | 123              | 100      |            |                  |          |
| 4800       | 127              | 5        |            |                  |          |
| 4900       | 129              | 15       |            |                  |          |
| 5000       | 131              | 30       |            |                  |          |
| 5100       | 132              | 10       |            |                  |          |
| 5200       | 133              | 50       |            |                  |          |
| 5300       | 133              | 75       |            |                  |          |
| 5400       | 134              | 40       |            |                  |          |
| 5500       | 135              | 0        |            |                  |          |

## PREVIOUS STUDIES OF THE BASIN GEOTHERMICS

Geothermal gradient maps of the Niger Delta have been constructed by Nwachukwu (1976), Avbovbo (1978) and Evamy *et al.*, (1978). Nwachukwu (1976) examined 100 well logs and observed that the central portion of the Delta has the lowest gradient of 0.7 to 1.0°F/100ft, and increases in all directions to about 3°F/100ft in the Cretaceous rocks in the north. Evamy *et al.* (1978) showed that thermal gradient increases with diminishing sand

percentage from 1.84°C/100m in the continental sands to 2.73°C/100m in the paralic section to a maximum of 5.47°C/100m in the shaly portion of the Niger Delta. Ovbovbo (1978) reported of 1.40°F/100ft in the Port Harcourt area of the Niger delta. The geothermal gradient in the distal part of the Niger Delta was calculated by Chukwueke *et al.* (1992) shows variation between 1.90°C/100m and 3.20°C/100m. Uko (1996) calculated geothermal gradient for the northern Niger Delta to vary between 1.526°C/100m and 2.727°C/100m. Akpabio (1998) reported that geothermal gradients are lowest (0.82°C/100m) at



(d) Well-AA-4

| Depth (ft) | Temperature (°F) | Sand (%) | Depth (ft) | Temperature (°F) | Sand (%) |
|------------|------------------|----------|------------|------------------|----------|
| 0          | 80               | 100      | 6400       | 147              | 20       |
| 0 - 2900   | -                | 100      | 6500       | 147              | 15       |
| 3000       | -                | 90       | 6600       | 148              | 30       |
| 3100       | -                | 95       | 6700       | 148              | 10       |
| 3200       | -                | 100      | 6800       | 149              | 50       |
| 3300       | 108              | 85       | 6900       | 151              | 40       |
| 3400       | 109              | 100      | 7000       | 151              | 70       |
| 3500       | 110              | 95       | 7100       | 152              | 90       |
| 3600       | 111              | 75       | 7200       | 153              | 30       |
| 3700       | 112              | 65       |            |                  |          |
| 3800       | 112              | 55       |            |                  |          |
| 3900       | 113              | 50       |            |                  |          |
| 4000       | 115              | 0        |            |                  |          |
| 4100       | 116              | 30       |            |                  |          |
| 4200       | 117              | 45       |            |                  |          |
| 4300       | 119              | 10       |            |                  |          |
| 4400       | 121              | 30       |            |                  |          |
| 4500       | 123              | 45       |            |                  |          |
| 4600       | 127              | 15       |            |                  |          |
| 4700       | 129              | 50       |            |                  |          |
| 4800       | 132              | 0        |            |                  |          |
| 4900       | 133              | 30       |            |                  |          |
| 5000       | 133              | 45       |            |                  |          |
| 5100       | 132              | 10       |            |                  |          |
| 5200       | 133              | 30       |            |                  |          |
| 5300       | 133              | 45       |            |                  |          |
| 5400       | 132              | 15       |            |                  |          |
| 5500       | 133              | 60       |            |                  |          |
| 5600       | 137              | 10       |            |                  |          |
| 5700       | 139              | 0        |            |                  |          |
| 5800       | 139              | 0        |            |                  |          |
| 5900       | 139              | 6        |            |                  |          |
| 6000       | 141              | 100      |            |                  |          |
| 6100       | 142              | 70       |            |                  |          |
| 6200       | 142              | 85       |            |                  |          |
| 6300       | 146              | 40       |            |                  |          |

the central of the Delta and increases both seawards and northwards up to 2.62°C/100m and 2.95°C/100m respectively in the continental sands of Benin Formation. In the paralic Agbada deposition, geothermal gradients ranges from 1.83°C/100m to 3.0°C/100m at the central part, highest values of 4.6°C/100m is seen northwards, while intermediate value of 2.5°C/100m is recorded seawards.

## DISCUSSION

In this study, the geothermal gradient is obtained based on the assumption of a linear increase of temperature with depth. Estimations of the segmented thermal gradients have been obtained from the slopes of the linear segments. The temperature-depth profiles of all the four

wells studied in this work have characteristic two principal line segments.

For the well AA-1, Fig. 4a, which was logged to the depth 6500 ft (1981m), it was observed that it can be classed into only two distinct parts, an upper part up to 5000 ft (1524m) and the lower part from 5000 ft to 6500ft. The geothermal gradients for these two parts have been estimated to be 1.22°F/100ft (2.220°C/100m) and 1.87 °F/100ft (3.403°C/100m) respectively. It is therefore observed that there is a gradient shift between 1524m and about 1981m. A shift that is estimated to be 0.65°F/100ft (1.183°C/100m).

This shows that in this well there is a gradual increase in temperature with depth, up to about 1524.00m. This depth could be correlated lithologically to the Benin sandy formation. And

thereafter a geothermal gradient increase is observed bringing about a new gradient from the depth of about 1524m downhole. This lower part from about 1524m may have resulted from an increase in shale unit and therefore could be correlated to the Agbada sand-shale intercalation.

For well AA-2, Fig. 4b, we observed two distinct parts in the thermal profile first an initial part (0-5400ft) and the lower segment (5400 – 8500ft). The upper segment has a gradient of 2.22°C/100m (1.22°F/100ft), the lower part has a geothermal gradient estimated to be 2.421°C/100m (1.33°F/100ft). We surmise from our observations in this well that the sandy formation reaches up to about 5400ft (1646m) while the sand-shale intercalation formation is seen from this marker to a depth of 8500ft.

For well AA-3, Fig. 4c, we again observed two distinct line segments. An initial part (from 0 to 4800ft), and the lower part (from 4800 to 7200ft). The geothermal gradient for these two parts have been also estimated to be 0.80°F/100ft (1.456°C/100m) and 1.47°F/100ft (2.675°C/100m) respectively.

Well AA-4, Fig. 4d, also has the characteristic two line segments as in the other wells. The first part (from 0 to 4400 ft) has a geothermal gradient of 0.86°F/100ft (1.565°C/100m), the second line segment (4400 to 7200ft) has a gradient of 0.92°F/100ft (1.674°C/100m).

From our results, one trend is evident: gradients in the upper sandy Benin Formation is lower than in the shaly Agbada Formation. The Akata Formation was not encountered in the Wells under study.

There is an observed increase in geothermal gradient with depth. This of course is in conformity with existing literatures (Bassiouni, 1994; Parasnis, 1975; and Speece *et al.*, 1985).

The question is, therefore, why there are two temperature line segments for the Wells? It is suggested here, that this could have been due to some thermal disturbances such as fluid flow in the continental sands of the Benin Formation. Ground water flow in the Niger Delta can be interpreted as occurring in two distinct zones. There is the upper meteoric zone where flow is controlled by topography. Meteoric groundwater recharges by precipitation and discharges to the major systems (Back, 1966; Smith *et al.*, 1983) and the Atlantic Ocean. Meteoric effects are important down to several kilometers depth onshore, but could be non-existent far offshore (Blanchard, 1987). The compactional or geopressured zone underlies the meteoric system. Groundwater flow is controlled by excess pore-fluid pressure gradients that are generated by several processes and dissipated as sediments consolidate. The major cause of geopressing is delayed compaction created by low sediment permeability (Gibson, 1958; Jones, 1969; Magara, 1976; Sharp and Domenico, 1976; Keith and Rimstidt, 1985). Other mechanisms for geopressing have been proposed (Burst, 1969; Weaver and Beck, 1971; Barker, 1972; Bruce, 1984 and Hedberg, 1980). It is possible that the higher geothermal gradient in the Agbada Formation could be associated with geopressured zone, which could be caused by loss of sands. These effects are presently speculative because there were no geopressure data.

Furthermore the most likely reasoning for the two temperature line segments is that there is a great variation in the lithological composition of the Wells. Segments of low thermal gradients correspond with depths of high sand percentage, Figures 4. Sands are better conductors than shale. The vertical view also shows that

Table 2: Bottom-hole-temperatures with Depth for Wells AA-1, AA-2, AA-3 and AA-4

| WELLS     | DEPT (FEET) | TEMPERATURE (°F) |
|-----------|-------------|------------------|
| Well AA-1 | 0           | 80               |
|           | 5000        | 137              |
|           | 6500        | 173              |
| Well AA-2 | 0           | 80               |
|           | 5400        | 145              |
|           | 8500        | 196              |
| Well AA-3 | 0           | 80               |
|           | 4100        | 113              |
|           | 7200        | 153              |
| Well AA-4 | 0           | 80               |
|           | 4200        | 117              |
|           | 7200        | 153              |

geothermal gradient increases as sand percentage decreases. There is a continuous but not linear relationship between geothermal gradients and depth from 1.03 °F/100ft in the continental sands to 1.40 °F/100ft in the marine paralic sand-shale section. These figures, of course, lead to the thermal conductivity variation. Shales have been known to exhibit some form of thermal insulation than sand stones and vice versa. Consequently shales have higher temperatures than sandstones.

## CONCLUSION

Analysis of continuous temperature-log data from southeast Niger Delta indicates that lithology affects geothermal gradients. There is an increase in gradient in the areas of high shale composition, hence a relationship between temperature and lithology is established. The low geothermal gradient corresponds to the upper sandy Benin Formation, having values which ranges between 0.80 °F/100 ft (1.456 °C/100m) and 1.22 °F/100 ft (2.220 °C/100m) with an average of 1.03 °F/100 ft (1.875 °C/100m). For the shaly Agbada Formation segment, the temperature gradient ranges between 0.92 °F/100 ft (1.674 °C/100m) and 1.87 °F/100ft (3.403 °C/100m) with an average of 1.40 °F/100ft (2.548 °C/100m). The depths of Benin formation was observed to vary between 4200 ft (1280 m) and 5400ft (1879 m).

Evidence of fluid dynamics and geopressures as supportive regional heat-transport processes is not available. Analysis of the geothermal pattern indicates that thermal conductivity variations, created by lithology variation could be a contributing factor for the regional heat transportation. The geothermal gradients estimated are in agreement with those of earlier works carried out by Nwachukwu (1976), Avbovbo (1978), Uko (1996) and Akpabio (1998).

The temperature distribution is actually a curve, not linear, for deep wells (Table 2, Figure 5). The curve can be approximated by a linear segment in the upper section of the well. The lower part of the curve can be approximated by a linear segment. Representing temperature distribution of formation with two linear segment as in this research is valid.

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