



## Article Info

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## Goelectrical Assessment of Groundwater Potential within Zamfara and its Environs, Northwestern Nigeria

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Groundwater potential assessment was carried out within Zamfara environs, Northwestern Nigeria using goelectrical technique with a view of solving the problem of incessant failure of boreholes in the study area. A total of one hundred and eighty-three (183) vertical electrical soundings (VES) were used to identify potential groundwater bearing zones capable of sustaining economic development of the study area. Two hydrogeological units were investigated (basement rock units and sedimentary rock unit), using Omega resistivity meter Model No. 122, to measure and record the resistance of the subsurface by Schlumberger configuration. The data obtained were interpreted quantitatively and qualitatively using the partial curve matching and computer iteration techniques to generate the first order goelectric parameters. Generally, the VES result from the basement rock units revealed, four goelectric layers which correspond to lateritic top soil, weathered basement (clay), partially fractured layer/fractured layer and fresh basement. The weathered/fractured layer was identified as the water bearing layer, within the basement rock units of the study area. From geospatial analysis of both weathered thickness/fracture thickness layers, South and Northeastern part tends to be the most prospective area with the best hydrogeologic conditions for borehole siting within the basement rock units. Consequently, three geo-electric layers were delineated from VES result obtained from Gundumi formation, which correspond to sandy clayey top/gravelly sandy top soil, second layer are mostly silty-clay/compacted sandstone/sandy gravel layers, the third layer were majorly saturated sandstone in some instances silty clay. However, the aquiferous layer is saturated sandstone/sandy gravel layer. The Dar Zarrouk result revealed excellent groundwater potential within the Gundumi formation. The values of coefficient anisotropy obtained from Gundumi rock units range from 0.44 to 3.79, which implies moderate saturation of groundwater. This is an indication that the aquifers of the Gundumi formation is more promising and it can be tap for both domestic and agricultural uses.

**Keywords:** Vertical electrical sounding, Fractured layer, Saturated Sandstone, Basement rock units, Gundumi formation.

## 1. Introduction

Groundwater exploration is gaining more and more importance in Nigeria owing to the ever increasing demand for water supplies, especially in areas with inadequate surface water supplies. Already, ten percent of the world's population is affected by chronic water scarcity and this is likely to rise to one third by about 2025 (Coker, 2012). High increases in industrial development, urbanization and agricultural production have resulted in freshwater shortages in many parts of the world. As a result of this increasing demand for portable water for these various purposes, there is need to have a planned and optimal utilization of water resources. Aquifer parameter is necessary for the management of

groundwater resource. The parameters necessary for the description of the dynamics of aquifer, include, geometry of the pore space, geometry of the rock particles, secondary geologic processes such as faulting and folding. These parameters jointly affect the rate and pattern of groundwater flow (Udoinyang and Igboekwu, 2012).

The ease of developing groundwater in Nigeria is restricted by the fact that most parts of the country are underlain by Basement Complex rocks. (Kazeem, 2007). Development of secondary porosity and permeability by weathering in such terrains bring about the

occurrence of groundwater. The aquifers are inherently discontinuous; hence, the need to conduct geophysical investigation to locate areas with abundance of such fractures capable of holding economic quantity of water in place for productive borehole placement.

Groundwater could be found in either basement or sedimentary terrains of the study area. Basement rock lacks a defined primary porosity but possesses secondary porosity with the presence of joints, fracture and fault. Most sedimentary rocks serve as good aquifers because they possess primary porosity and their pores spaces are interconnected. These two factors (the primary porosity and the rock unit permeability) determine whether a unit of rock can serve as a good aquifer.

Olawuyi and Abolarin, (2013) Alabi *et al.*, (2013) and Badmus and Olatinsu (2010) note that the characteristics of basement aquifer vary with the mode of geological formation, mineralogical composition and structure of the substrate as well as the topography in which they occur. Generally, fractured crystalline rocks yield smaller quantities of groundwater in many environments in comparison with sedimentary aquifer. This makes it an important resource which can act as a natural storage that can buffer against shortages of surface water, as in during times of drought. Groundwater is naturally replenished by surface water from rivers when this recharge reaches the water table.

The Vertical Electrical Sounding (VES) is a geophysical method for measuring vertical variations of electrical resistivity due to inhomogeneity in the subsurface. The method has been recognized to be more appropriate for hydrogeological study of sedimentary basin and that crystalline environment.

Its wide applicability is associated with the simplicity of instrumentation. Also, the field logistics are easy and straight forward while the analyses of the sets of acquired data are less tedious and economical (Olowofela *et al.*, 2005; Batayneh, 2009; Ezeh and Ugwu, 2010; Ologe *et al.*, 2014).

Several researchers have carried out systematic hydrogeological and geophysical studies in the different region of the world (Bose and Ramakrishna 1978; Singhal 1997; Rai *et al.*, 2011; Adeoti and Uchegbulam, 2010; Ratnakumari *et al.*, 2012; Rai *et al.*, 2013) to delineate aquifers and the occurrence and movement of groundwater in

intertrappeans/vesicular and fractured zones within the trap sequence and sedimentary formations below the traps, which are considered to be a potential source of groundwater.

The area under investigation is fast growing in terms of population and business activities. It is characterized by the shortage of potable water suitable for domestic and economic purposes. Virtually all the hand dug wells dry up during the dry season, mostly within the dominant basement terrain, which might be due to the nature of the patch aquifers. Thus, there is a great problem of locating prolific aquifers in different parts of the study area. Hence, there is need to find good quality water source(s) must be found for the residents of this area with a view to saving communities from shortage of water supply and unknown health hazards. To address these challenges, Electrical resistivity methods of geophysical prospecting might be very useful.

In this study, the vertical electric sounding using Schlumberger array was employed to investigate the groundwater potential of Zamfara State to assist in planning, improvement and management of the groundwater resource of the area.

### 1.1 Study Area

This research covers the entire Zamfara State with estimated area coverage of 39,762 Km<sup>2</sup>, within the NW Nigeria (Figure 1), with latitude 7°18'13.709"E to 10°49'4.152"N and Longitude: 5°1'27.638"E to 13°10'45.537"N. The study area belongs to the Sudan savannah region of Africa; an area mostly affected by droughts (Figure 1).

Temperatures are generally extreme, with average daily minimum of 18°C, during cool months of December and January and in the hottest months of April to June, an average maximum of 38°C and minimum of 24°C temperatures are recorded.

Rainfall is generally low; the average annual rainfall ranges from 600 to 1000 mm across the entire State (Nigeria Meteorological Agency, 2020). Much of the rain, falls between the months of May to September, while the months of October to April experienced little or no rainfall. Evaporation is high, ranging from 80 mm in July to 210 mm in April to May (Nigeria Meteorological Agency, 2020).

A monthly average evapo-transpiration range of about 140 mm represent 30 of monthly average precipitation into the catchment.

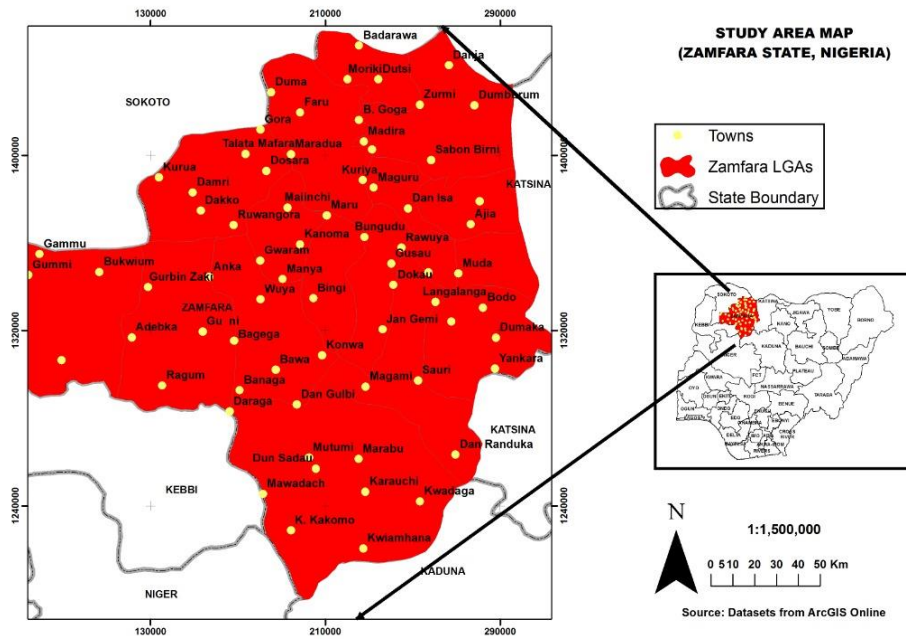


Figure 1. Map of the Study Area

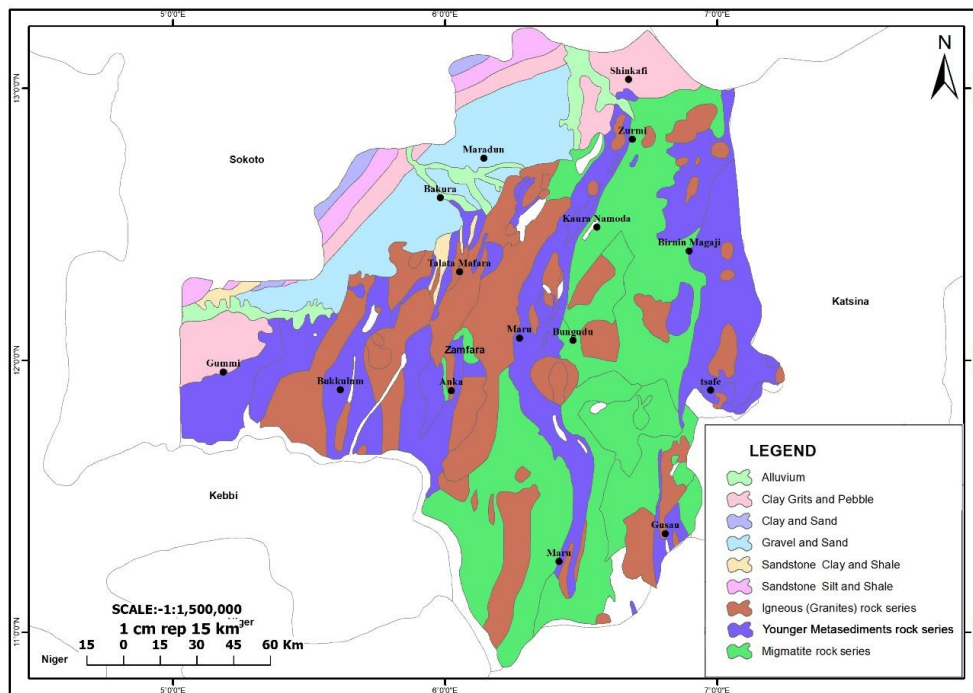


Figure 2. General Geological Map of Zamfara State, (Nigeria Geological Survey Agency, 2006).

**1.2 Geological Setting of the Study Area**

About 90% of the State is underlain by a variety of crystalline rocks of the basement complex of north western Nigeria described by McCurry (1976) to be composed largely of gneiss, schist,

migmatite, granite and granodiorite (Figure 2). The structural features commonly exhibited by the basement rocks include foliation, lineation, folds, rock-rock contacts, faults and joints. The rest of the state is occupied by the oldest sediments of the Sokoto (Illullemeden) basin

described by Oteze (1976) and Kogbe (1976). Groundwater in the basement rocks of the state are mainly sourced from fractures and joints and in the intergranular pores of fine to coarse (white or light grey) sand or gravel in the sedimentary areas (Oteze, 1976).

About 10% of the State is underlain by Gundumi formation which consists of clays, sandstones and pebble beds, thought to be lacustrine and fluvial in origin (Figure 2). Its maximum thickness is reported to be up to 300 m, near the Niger border (Anderson and Ogilbee, 1973). The base is marked by conglomeratic beds which are well preserved and exposed by the road side at Tureta and Ruwan Kalgo (Kogbe, 1976). These basal beds contain rounded quartz cobbles and pebbles and attain a thickness of about 3m. The formation is the oldest sedimentary rocks in the Northern parts of the basin it, lies uncomfortably on the Basement Complex. Other exposures of the Formation are found by Rivers Zamfara and Dutsin Dambo, near Bakura. The indication, from borehole sections, is that the basal conglomerates are overlain by beds which are more argillaceous from the bottom to the top.

## 2. Methodology

A total of one hundred and eighty-three (183) Vertical Electrical Sounding (VES) points were carried out within the study area using Schlumberger array with Omega resistivity meter Model No. 122, to measure and record the resistance of the subsurface. The VES stations were systematically selected at different locations based on the major rock units within the study area.

The potential electrodes remain fixed and the current electrodes were expanded simultaneously about the center of the spread. The maximum electrode separation used was  $AB/2 = 100$  m and a maximum potential electrode spacing  $MN/2 = 0.5$  m which are normally arranged in a straight line, with the potential electrode placed in between the current electrodes. This configuration is mostly used as it would provide sub-surface information considering the depth of penetration. The field data were converted to apparent resistivity ( $\rho$ ) in ohm-meter by multiplying with Schlumberger geometric factor ( $k$ ). The sounding curve for each point was obtained by plotting the apparent resistivity on the ordinate against half electrode spacing on a bilogarithmic paper and edited in the Interpex 1-D software until a smooth layered model with a minimum percentage error of  $<1$  is gotten in which a model graph is plotted for each VES point (Figure 3.7a-c). The curves obtained were then compared to the H, K, Q, and A curve types. Dar-Zarrouk parameters (Longitudinal

conductance) were used to define target areas of groundwater potential and also used in aquifer protection studies within the sedimentary section of the study area. The total longitudinal conductance values were utilized in evaluating the overburden protective capacity of the area underlain by sedimentary formation. This is because the earth medium acts as a natural filter to percolating fluids.

**Dar Zarrouk Parameters:** some parameters are generally very important in the understanding and interpretations of geological model (Egbai and Iserhein-Emekeme, 2015). These parameters are related to different combination of the thickness and resistivity of each geoelectric layers in the model (Braga *et al*, 2006). For a sequence of horizontal, homogeneous and isotropic layers resistivity  $\rho_i$  and thickness  $h_i$ , the Dar Zarrouk parameters (longitudinal conductance  $S$  and transverse resistance  $T$  are respectively defined as:

$$S = \sum_{i=1}^n \frac{h_i}{\rho_i} \quad 1$$

$$T = \sum_{i=1}^n h_i \rho_i \quad 2$$

If the total thickness of the layers in the geoelectric section considered is  $h$ , then the average longitudinal resistivity  $\rho_L$  is given by

$$\rho_L = \sum_{i=1}^n \frac{h_i}{S_i} \quad 3$$

And the average transverse resistance  $\rho_t$  is given by

$$\rho_t = \sum_{i=1}^n \frac{T_i}{h_i} \quad 4$$

$\rho_i$  is always greater than  $\rho_L$ . Therefore, the entire section will thus be anisotropic with regards to electrical resistivity. The coefficient of electrical anisotropy is defined as:

$$\lambda = \sqrt{\frac{\rho_t}{\rho_L}}$$

Where  $\lambda$  is real and greater than 1.

The reflection coefficient ( $R_c$ ) and resistivity contrast ( $F_c$ ) of the fresh basement rock of the study area was calculated using the method of Oladunjoye and Jekayinfa (2015).

$$R_c = \frac{\rho_n - \rho_{n-1}}{\rho_n + \rho_{n-1}}$$

And

$$F_c = \frac{\rho_n}{\rho_n - 1}$$

Where  $\rho_n$  is the layer resistivity of the  $n$ th layer and  $\rho_{n-1}$  is the layer resistivity overlying the  $n$ th layer. The Dar Zarrouk parameters of the study area were evaluated based on the weathered layer thickness, resistivity of overburden thickness, transverse resistance (T), coefficient of electrical anisotropy ( $\lambda$ ), reflection coefficient (Rc) and resistivity contrast (Fc). Values of various formation parameters are in table 6.

ArchGIS 10.0 was used to generate Iso-patch contour map, fracture depth map, and groundwater potential map of the study area.

### 3. Results and Discussion

The Vertical Electrical Soundings (VES) data were interpreted qualitatively and quantitatively. The results show details of the measured parameters such as thickness of layers, resistivity of layers, fitting error and curve-type for all the sounded points and including transverse resistance, longitudinal conductance for the sedimentary terrain. From the curve type distribution of the 183 VES in the study area

(table 1, 2 3 & 4). There are about three to four (4) different geo-elctetric layers.

A total of thirty-seven (37) Vertical Electrical Sounding (VES) points were conducted within the older metasedimentary rocks in the studied area and the results interpretation revealed three subsurface layers, the top layer which mainly composed of laterite, sandy soil and in some instance clayey, the thickness of this layer range from 0.5 to 8.5m with resistivity (ohm-m) value of 265.7  $\Omega$ m and 287  $\Omega$ m respectively. The weathered layer range in thickness between 1.8 to 22.9 m with resistivity value of 34.3  $\Omega$ m and 130  $\Omega$ m respectively. While the fractured thickness range between 31.2 to 90 m with resistivity value of 193.4  $\Omega$ m and 2844.5  $\Omega$ m respectively. Table 5 show the statistics of curve types of the studied VES data, the older metasediments revealed H, KH, Q, AK, K and HK-curve type with H-curve type being the dominant (table 1).

The aquiferous layers are majorly partly fractured with some well fractured layers, however weathered layer equally serve as aquifer within this rock units (table 1). This is typical of crystalline environment.

**Table 1.** Summary of Vertical Electrical Sounding within Older Metasediments (showing aquiferous layers)

| VES Locations | Layer/Curve Type | Resistivity ohm-m | Thickness (m) | Depth (m) | Layer Characteristics       |
|---------------|------------------|-------------------|---------------|-----------|-----------------------------|
| 1             | Q                | 24.1              | 31.2          | 45        | Fractured Basement (Schist) |
| 2             | H                | 193.4             | 38.2          | 45        | Fractured basement          |
| 3             | Q                | 707.4             | 5.8           | 6.6       | Weather (Lateritic layer)   |
| 4             | Q                | 55                | 36.9          | 80        | Fractured basement          |
| 5             | H                | 57.1              | 20.9          | 24.1      | weathered Basement (Clay)   |
| 6             | H                | 29.3              | 29.2          | 32.2      | weathered Basement (Clay)   |
| 7             | H                | 2844.5            | 82.6          | 90        | Fractured basement          |
| 8             | A                | 118.1             | 18.8          | 90        | Partly fractured            |
| 9             | A                | 250.7             | 54.2          | 60        | Fractured basement          |
| 10            | H                | 206.8             | 41.2          | 50        | Fractured basement          |
| 11            | H                | 161.5             | 31.4          | 60        | Fractured basement          |
| 12            | H                | 229.7             | 42.9          | 60        | Fractured basement          |
| 13            | A                | 222.3             | 73.3          | 80        | partly fractured basement   |
| 14            | H                | 691.8             | 74.9          | 50        | partly fractured basement   |
| 15            | KH               | 249.2             | 77.6          | 80        | partly fractured basement   |
| 16            | H                | 79.5              | 78.1          | 80        | partly fractured basement   |
| 17            | HK               | 32.7              | 71.5          | 80        | partly fractured basement   |



|    |    |       |      |      |                             |
|----|----|-------|------|------|-----------------------------|
| 18 | H  | 264.7 | 74.6 | 90   | partly fractured basement   |
| 19 | H  | 690.6 | 72.4 | 80   | partly fractured basement   |
| 20 | A  | 556.3 | 75.6 | 80   | partly fractured basement   |
| 21 | AK | 219.2 | 65.8 | 80   | partly fractured basement   |
| 22 | H  | 353.7 | 37.8 | 50   | partly fractured basement   |
| 23 | AK | 261   | 79   | 80   | partly fractured basement   |
| 24 | H  | 300.6 | 77   | 80   | partly fractured basement   |
| 25 | HA | 748.2 | 74.1 | 80   | partly fractured basement   |
| 26 | HA | 675.6 | 66.6 | 70   | partly fractured basement   |
| 27 | AK | 727.7 | 60.8 | 70   | partly fractured basement   |
| 28 | H  | 410.7 | 72   | 80   | partly fractured basement   |
| 29 | HK | 121.8 | 71.6 | 80   | partly fractured basement   |
| 30 | KH | 207.6 | 9.4  | 47.4 | fractured basement          |
| 31 | H  | 16.6  | 34   | 52   | fractured basement          |
| 32 | HK | 85.2  | 35   | 52.3 | fractured basement          |
| 33 | A  | 1213  | 12.6 | 22.1 | slightly fractured basement |
| 34 | KH | 121   |      |      | fractured zone              |
| 35 | H  | 195   | 15   | 41.5 | fractured zone              |
| 36 | H  | 180.2 | 12.3 | 23.5 | fractured basement          |
| 37 | A  | 36.6  | 21.1 | 26.5 | fractured basement          |

A total of forty-five (45) Vertical Electrical Sounding (VES) points were conducted within younger metasediments rock units and the result interpretation revealed three subsurface layers, the top layer which mainly composed of laterite, sandy soil and in some instance clayey, the thickness of this layer range from 1 to 2.8 m with resistivity value of 172.9  $\Omega$ m and 133 $\Omega$ m respectively. The weathered layer range in thickness between 4.1 to 31.8m with resistivity value of 38.9  $\Omega$ m and 85.9 $\Omega$  m respectively.

While the fractured thickness range between 8 to 90m with resistivity value of 257  $\Omega$ m and 558.1  $\Omega$ m respectively (Table 2). The interpreted VES data for this rock unit revealed H, A, KH, Q, AK, K, HK and AH-curve.

The aquiferous layers are majorly well fractured layers, however weathered layer equally serve as aquifer (well saturated with anticipated moderate yielding capacity) within this rock units (table 2).

**Table 2.** Summary of Vertical Electrical Sounding within Younger Metasediments (showing aquiferous layers)

| VES Locations | Layer/Curve Type | Resistivity ohm-m | Thickness (m) | Depth (m) | Layer Characteristics       |
|---------------|------------------|-------------------|---------------|-----------|-----------------------------|
| 1             | Type H           | 30.9              | 5.7           | 7.2       | weathered basement (clay)   |
| 2             | Type AK          | 22.4              | 34.7          | 45        | Fractured basement (schist) |
| 3             | Type Q           | 24.1              | 31.2          | 45        | Fractured Basement (Schist) |

|    |         |         |      |      |  |
|----|---------|---------|------|------|--|
| 4  | Type QH | 41.3    | 11.5 | 13.3 | Weather (Clayey layer)<br>fractured Basement<br>(Schist) |
| 5  | Type K  | 72.7    | 38.2 | 80   | weathered basement                                       |
| 6  | Type H  | 79.6    | 14.8 | 18.5 | Fractured basement                                       |
| 7  | Type H  | 142.7   | 52.1 | 60   | Fractured basement                                       |
| 8  | Type H  | 183     | 40.9 | 50   | Fractured basement                                       |
| 9  | Type A  | 98.1    | 38.7 | 60   | Fractured basement<br>(schist)                           |
| 10 | Type A  | 91.8    | 42.4 | 60   | Fractured basement<br>(schist)                           |
| 11 | Type HA | 462.2   | 34.2 | 50   | Fractured basement                                       |
| 12 | A       | 462.3   | 2.6  | 6.6  | Fractured Basement                                       |
| 13 | A       | 947     | 2.6  | 11.3 | Fractured Basement                                       |
| 14 | HA      | 186     | 6.7  | 10.5 | Weathered Layer  |
| 15 | AK      | 100000  | 17.6 | 18.4 | Fractured Basement                                       |
| 16 | A       | 14965.6 | 6    | 7.2  | Fractured Basement                                       |
| 17 | AH      | 498.8   | 78.8 | 80   | partly fractured<br>basement                             |
| 18 | QH      | 176.5   | 72.2 | 80   | partly fractured<br>basement                             |
| 19 | QH      | 1280.8  | 71.6 | 80   | partly fractured<br>basement                             |
| 20 | HK      | 162.8   | 52   | 60   | partly fractured<br>basement                             |
| 21 | A       | 91.1    | 73.2 | 80   | partly fractured<br>basement                             |
| 22 | A       | 6835.4  | 87.8 | 90   | partly fractured<br>basement                             |
| 23 | H       | 2250.3  | 67   | 80   | partly fractured<br>basement                             |
| 24 | H       | 524.9   | 75.4 | 80   | partly fractured<br>basement                             |
| 25 | H       | 319.9   | 38   | 50   | partly fractured<br>basement                             |
| 26 | AH      | 307.7   | 76.4 | 80   | partly fractured<br>basement                             |
| 27 | QH      | 216.9   | 41.6 | 50   | partly fractured<br>basement                             |
| 28 | H       | 173.8   | 62.3 | 70   | partly fractured<br>basement                             |
| 29 | A       | 322.7   | 56.2 | 80   | partly fractured<br>basement                             |
| 30 | H       | 852.8   | 76.8 | 80   | partly fractured<br>basement                             |
| 31 | KH      | 169.6   | 72   | 80   | partly fractured<br>basement                             |
| 32 | KH      | 487.9   | 74.1 | 80   | partly fractured<br>basement                             |
| 33 | H       | 545.7   | 74.1 | 80   | partly fractured<br>basement                             |
| 34 | KH      | 235.4   | 48.2 | 80   | partly fractured<br>basement                             |
| 35 | HK      | 558.1   | 55.9 | 80   | partly fractured<br>basement                             |
| 36 | H       | 240.3   | 13.7 | 25.8 | fractured basement                                       |

|    |    |       |      |      |  |
|----|----|-------|------|------|--|
| 37 | AK | 163.8 |      |      | fractured basement<br>partly fractured<br>basement |
| 38 | HK | 87.8  | 28.1 | 35.8 |  |
| 39 | H  | 257   | 8    | 13.4 | fractured basement                                 |
| 40 | KH | 180.8 |      |      | fractured basement                                 |
| 41 | H  | 40    | 3    | 10   | fractured basement                                 |
| 42 | H  | 45.9  | 3.9  | 15.5 | fractured basement                                 |
| 43 | H  | 63.4  | 5.4  | 16.8 | fractured basement                                 |
| 45 | K  | 129.2 |      |      | fractured basement                                 |

A total of sixty-two (62) Vertical Electrical Sounding (VES) were conducted within the Pan-African granites and the result revealed three subsurface layers, the top layer which mainly composed of topsoil, laterite, and sandy and in some instance clayey, the thickness of this layer range from 0.9 to 3.7m with resistivity value of 43.5  $\Omega$ m and 69.3  $\Omega$ m respectively. The weathered layer range in thickness between 2.9 to 24.3m with resistivity value of 38.9  $\Omega$ m and 186.3  $\Omega$ m respectively. While the fractured thickness range between 35.8 to 90m with resistivity value of 605.7  $\Omega$ m and 264.7  $\Omega$ m respectively (Table 3). Biotite Gneiss forms the country rock, above which laterite is noted. Resistivity values of less than 500  $\Omega$ m are reported from 55% of stations but 45% of stations are having values between 500  $\Omega$ m and 1000  $\Omega$ m. Those stations where resistivity values

are less than 1000  $\Omega$ m are representing the deeper and fractured coarse biotite granites formations.

**Fresh Basement:** This represents the deepest layer which is semi-infinite with resistivity ranges between 51.5 to 3621  $\Omega$ m within the study area. It is not a source of groundwater unless fractured. Its ability to conduct electrical current arises mainly from their porosity, permeability and the fluid contained within the matrix. The development of secondary porosity by jointing and fracturing, results in a further reduction of the resistivity; consequently, the resistivity of water bearing formation decreases when highly saturated in most cases. However, there is a steady increase in resistivity, it probably indicates fresh basement rock without fractures. It is advisable to stop further probing.

**Table 3.** Summary of Vertical Electrical Sounding within Pan-African Granites (showing aquiferous layers)

| VES Locations | Layer/Curve Type | Resistivity ohm-m | Thickness (m) | Depth (m) | Layer Characteristics                                    |
|---------------|------------------|-------------------|---------------|-----------|--|
| 1             | H                | 245.1             | 40.3          | 45        | Fractured basement                                       |
| 2             | KH               | 849               | 1.2           | 1.8       | Weather (Lateritic layer)                                |
| 3             | Q                | 97.1              | 4.6           | 6.3       | Weather (Clayey layer)                                   |
| 4             | K                | 254.8             | 35.8          | 45        | Fractured Basement (Schist)<br>weathered basement (Clay) |
| 5             | H                | 16.2              | 11.7          | 17.6      |  |
| 6             | AK               | 53.1              | 32.7          | 80        | Fractured Basement<br>Fractured Basement                 |
| 7             | Q                | 54.9              | 33.9          | 80        | (schist)<br>Fractured Basement                           |
| 8             | Q                | 54.6              | 35.5          | 80        | (schist)<br>weathered Basement                           |
| 9             | H                | 36.3              | 18            | 21.7      | (Clay)<br>partly fractured                               |
| 10            | H                | 272.1             | 83.4          | 90        | basement   |
| 11            | H                | 418.2             | 87.5          | 90        | partly fractured<br>basement                             |
| 12            | H                | 605.7             | 35.8          | 60        | partly fractured<br>basement                             |
| 13            | HK               | 162.8             | 52            | 60        | partly fractured<br>basement                             |
| 14            | H                | 4027.5            | 75            | 90        | partly fractured   |



|    |        |         |      |     |  |                    |
|----|--------|---------|------|-----|--|--------------------|
|    |        |         |      |     |  | basement           |
| 15 | H      | 264.7   | 74.6 | 90  |  | partly fractured   |
| 16 | H      | 55.8    | 78.1 | 80  |  | basement           |
| 17 | HK     | 947.8   | 78.1 | 80  |  | partly fractured   |
| 18 | H      | 605.7   | 35.8 | 60  |  | basement           |
| 19 | H      | 452.3   | 78   | 80  |  | partly fractured   |
| 20 | AK     | 13.9    | 77.8 | 80  |  | basement           |
| 21 | HK     | 13.5    | 77.4 | 80  |  | partly fractured   |
| 22 | A      | 2349.1  | 72.6 | 80  |  | basement           |
| 23 | KH     | 292     | 71.5 | 80  |  | partly fractured   |
| 24 | H      | 2060    | 72.9 | 80  |  | basement           |
| 25 | H      | 1301.3  | 76.2 | 80  |  | partly fractured   |
| 26 | H      | 35      | 80.3 | 90  |  | basement           |
| 27 | H      | 279.3   | 54.8 | 60  |  | partly fractured   |
| 28 | H      | 745.4   | 69.7 | 70  |  | basement           |
| 29 | Type H | 17.3    | 3.2  | 4.2 |  | weathered basement |
| 30 | KH     | 1199.4  | 78.2 | 80  |  | partly fractured   |
| 31 | AK     | 374.2   | 75.6 | 80  |  | basement           |
| 32 | KH     | 576.6   | 78.2 | 80  |  | partly fractured   |
| 32 | AH     | 272.5   | 87.2 | 80  |  | basement           |
| 33 | A      | 449.4   | 73.6 | 80  |  | partly fractured   |
| 34 | H      | 632.3   | 47.1 | 50  |  | basement           |
| 35 | KH     | 15779   | 77   | 80  |  | partly fractured   |
| 37 | KH     | 487.9   | 74.1 | 80  |  | basement           |
| 38 | KH     | 270.9   | 34.9 | 50  |  | partly fractured   |
| 39 | H      | 662.9   | 78.8 | 80  |  | basement           |
| 40 | H      | 2242.7  | 67   | 80  |  | partly fractured   |
| 41 | H      | 925.2   | 67.2 | 80  |  | basement           |
| 42 | H      | 2883.4  | 76.8 | 80  |  | partly fractured   |
| 43 | H      | 391.1   | 66.1 | 70  |  | basement           |
| 44 | H      | 11982.2 | 62.9 | 70  |  | partly fractured   |
| 45 | A      | 256     | 50   | 80  |  | basement           |

|    |    |        |      |      |  |                         |
|----|----|--------|------|------|--|-------------------------|
|    |    |        |      |      |  | basement                |
|    |    |        |      |      |  | partly fractured        |
| 46 | H  | 1587.3 | 69.8 | 70   |  | basement                |
| 47 | A  | 140.5  | 29   | 52.1 |  | fractured basement      |
|    |    |        |      |      |  | slightly fractured      |
| 48 | H  | 321.4  | 10.1 | 16.9 |  | basement                |
| 49 | H  | 228.5  | 13.4 | 28.4 |  | fractured basement      |
| 50 | HA | 547.5  |      |      |  | fractured basement      |
| 51 | H  | 596.9  |      |      |  | fractured basement      |
| 52 | A  | 1151   | 23   | 43   |  | slightly fractured zone |
| 53 | HA | 16.8   | 23.5 | 56.8 |  | fractured zones         |
| 54 | H  | 21.2   | 23.7 | 53.7 |  | fractured zone          |
| 55 | H  | 54.7   | 14.5 | 44.7 |  | fractured zone          |
| 56 | H  | 21.4   | 26.5 | 38.8 |  | fractured zone          |
| 57 | H  | 523.1  |      |      |  | fractured basement      |
| 58 | H  | 320.9  |      |      |  | fractured basement      |
| 59 | H  | 172.5  |      |      |  | fractured basement      |
| 60 | A  | 145.6  |      |      |  | fractured basement      |
| 61 | H  | 52     | 20   | 52.5 |  | fractured zones         |
|    |    |        |      |      |  | slightly fractured      |
| 62 | A  | 3297.2 |      |      |  | basement                |

Thirty-eight VES was conducted within Gundumi Formation in order to delineate its groundwater potential. The results revealed three major layers that varies from sandy clayey top soil and in some instances gravels sand top soil while the second layers are mostly silty clay, compacted laterite, compacted sandstone and sandy gravels, the third layer were majorly sandstone, in some instance silty clay (Table 4). However,

where there exist a fourth layer silty clay or sandstone are mostly the delineated lithology.

The aquiferous units within this formation are mostly the saturated sandstone and sandy gravel layer as shown in table 4. Though, compacted sandstone when it possessed a secondary porosity via fracturing can equally yield enough water to the well.

**Table 4.** Summary of Vertical Electrical Sounding within Sedimentary Formation (showing aquiferous layers)

| VES Locations | Layer/Curve Type | Resistivity ohm-m | Thickness (m) | Depth (m) | Layer Characteristics | Longitudinal Conductance ( S) |
|---------------|------------------|-------------------|---------------|-----------|-----------------------|-------------------------------|
| 1             | Q                | 131               | 35.8          | 60        | saturated sandstone   | 0.32 (moderate)               |
| 2             | Q                | 189.4             | 34.7          | 60        | saturated sandstone   | 0.24 (weak)                   |
| 3             | Q                | 40                | 35            | 60        | saturated sandstone   | 1.01 (good)                   |
| 4             | H                | 200.9             | 32.9          | 60        | saturated sandstone   | 0.86 (good)                   |
| 5             | Q                | 44.8              | 37.9          | 60        | saturated sandstone   | 0.91 (good)                   |
| 6             | AK               | 87.1              | 29.8          | 60        | saturated sandstone   | 0.46 (moderate)               |
| 7             | Q                | 124.9             | 30.6          | 60        | saturated sandstone   | 0.32 (moderate)               |
| 8             | KH               | 238.8             | 27.9          | 60        | sandstone             | 0.76 (good)                   |
| 9             | A                | 270.9             | 19.3          | 27.1      | sandstone             | 0.82 (good)                   |
| 10            | H                | 158.5             |               |           | saturated sandstone   | 1.05 (good)                   |
| 11            | KA               | 3357              |               |           | sandstone             | 0.58 (moderate)               |
| 12            | H                | 1649              | 0.629         | 0.629     | gravels               | 0.35 (moderate)               |

|    |    |        |       |       |                     |                 |
|----|----|--------|-------|-------|---------------------|-----------------|
| 13 | H  | 83.2   | 34.42 | 40.6  | silty clay          | 0.47 (moderate) |
| 14 | HA | 98.5   | 28.71 | 34.8  | saturated sandstone | 0.58 (moderate) |
| 15 | H  | 1312   | 1.08  | 1.08  | garavels and sand   | 0.47 (moderate) |
| 16 | HK | 64     |       |       | silty clay          | 0.47 (moderate) |
| 17 | HK | 3067   | 7.8   | 13.4  | sandstone           | 0.47 (moderate) |
| 18 | K  | 1507   | 13.27 | 20.52 | compacted sandstone | 0.35 (moderate) |
| 19 | K  | 366    |       |       | saturated sandstone | 0.47 (moderate) |
| 20 | K  | 282    | 18.3  | 18.7  | sandstone           | 0.58 (moderate) |
| 21 | K  | 489    | 21.17 | 25.01 | sandstone           | 0.47 (moderate) |
| 22 | K  | 30.3   |       |       | saturated sandstone | 0.82 (good)     |
| 23 | K  | 165    |       |       | sandstone           | 0.35 (moderate) |
| 24 | K  | 38.2   |       |       | silty clay          | 0.35 (moderate) |
| 25 | K  | 1674   | 2.9   | 5.77  | sand and gravels    | 0.35 (moderate) |
| 26 | K  | 266    | 10.1  | 13.17 | sandstone           | 0.47 (moderate) |
| 27 | K  | 113.43 |       |       | sandstone           | 0.35 (moderate) |
| 28 | K  | 644    | 22.46 | 24.31 | sandstone           | 0.35 (moderate) |
| 29 | HQ | 75.7   | 30.9  | 54.5  | saturated sandstone | 0.47 (moderate) |
| 30 | H  | 436    | 49.1  | 52.3  | saturated sandstone | 0.47 (moderate) |
| 31 | K  | 354    | 42.5  | 52.3  | saturated sandstone | 0.47 (moderate) |
| 32 | K  | 354    | 41.8  | 52.3  | saturated sandstone | 0.47 (moderate) |
| 33 | HK | 242    |       |       | saturated sandstone | 0.70 (moderate) |
| 34 | K  | 354    | 41.8  | 52.3  | saturated sandstone | 0.47 (moderate) |
| 35 | K  | 407    |       |       | saturated sandstone | 0.47 (moderate) |
| 36 | H  | 488    |       |       | saturated sandstone | 0.47 (moderate) |
| 37 | K  | 354    | 41.8  | 41.8  | saturated sandstone | 0.35 (moderate) |
| 38 | HK | 242    |       |       | saturated sandstone | 0.35 (moderate) |
| 39 | H  | 189    | 15.4  | 27.2  | saturated sandstone | 0.47 (moderate) |

#### 4. Geospatial Analysis of VES Data of the Study Area

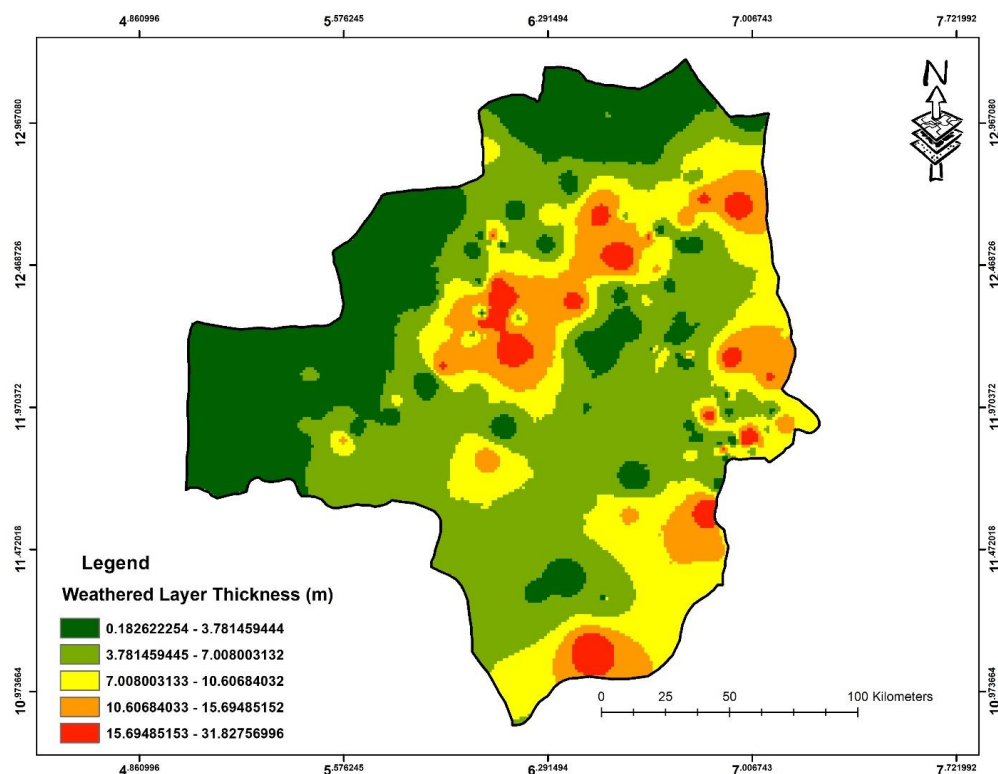
The resistivity of the second layer ( $\rho_2$ ) is the effect of fractured or weathered rocks (Figure 3 & 4). These layers determine whether the aquifer has groundwater potential or not. Figure 6 show the variation in weathered thickness across the area study area and it varies from 1.8 to 31.8m with average thickness of about 12m. For good groundwater yield in a well, Olayinka *et al*, 1997

suggested 20 – 30 m weathered thickness while Olorunfemi and Okhue, (1992) and Oladapo *et al.*, (2007) gave 25 m as the thickness of overburden that is viable for groundwater abstraction. The average thickness of weathered basement in the investigated area is 12m which is far less than the suggested average thickness in literatures. It is evident from the result that more than 50 % of the area is less than the value suggested and the only area that meets the value is south-eastern and the central part of the study area. However, most of the weathered

layer is either overlying a partly fractured layer or well fractured layer except in some few cases where it serves as the main aquifer layer.

From the apparent resistivity values, it is vivid that North-eastern and southern parts of the study area have much likelihood for good groundwater storage (figure 6). The resistivity ranges from 17.8 ohm-m and 600 ohm-m and

65% of stations out of 183 stations have shown the resistivity between 17.8 ohm-m and 500 ohm-m. The range of resistivity values between 500 ohm-m and 1000 ohm-m and that between 1500 ohm-m and 2500 ohm-m are 30% and 5% respectively. Whereas, the number of locations, having resistivity values greater than 2500 ohm-m are only 5 out of total 183 stations.



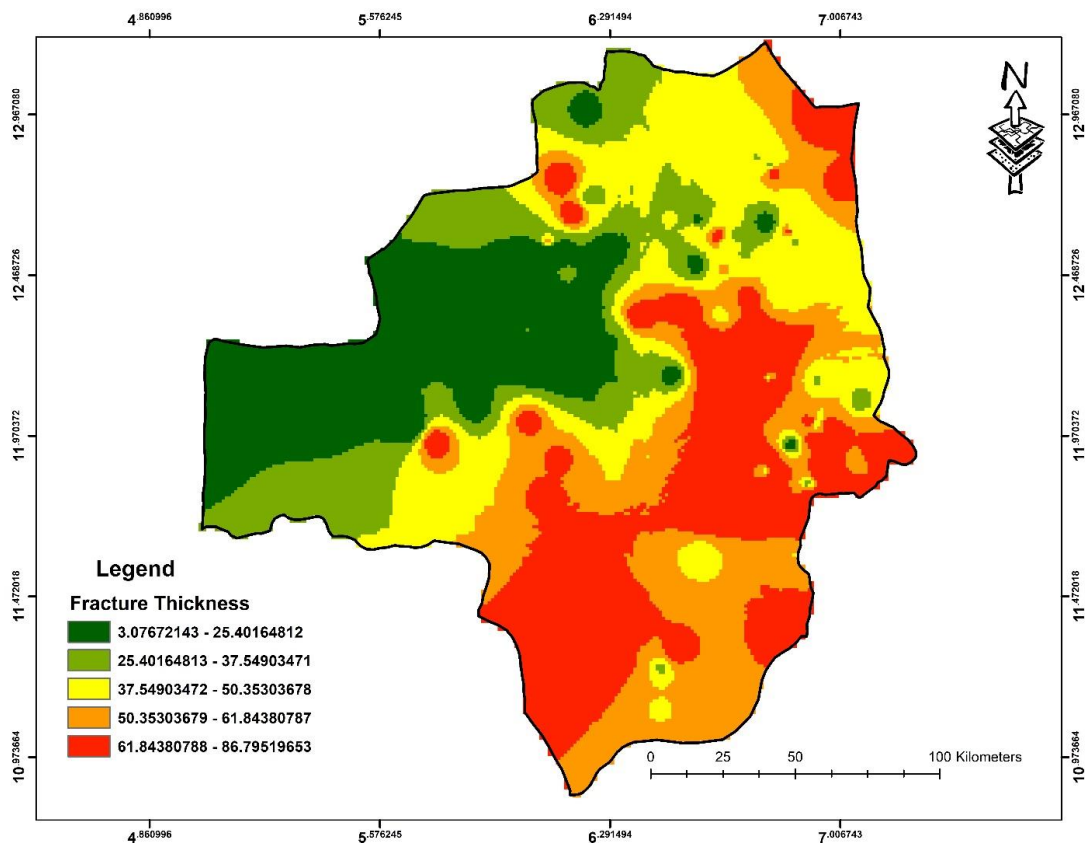
**Figure 3.** Weathered Thickness Map of the Study Area

Fracture is one of the factors that influence the occurrence of groundwater mostly in crystalline geologic environment. Consequently, the geospatial fractured map of the studied VES was produced from fractured thickness value as shown in figure 4. The map depicts intense fracturing at the N-E and S-W part of the study area. This equally revealed that the dominant structural trend of the studied area is in NE-SW direction. Thus form the basis for groundwater flow and storage capability (see figure 6).

Based on Olayinka *et al.*, 1997 and Oyedele and Olayinka (2012), classification of aquifer potential as a function of the basement rock, the basement rock can be classified as high fractured permeability as a result of fractured

layer with resistivity less than 750  $\Omega$ m which can be seen in the northeastern and the southeastern and northeastern parts of the area investigated which is an indication of good aquifer potential. Also, basement resistivity value from 750 to 1500  $\Omega$ m is classified as medium aquifer potential which has reduced influence of weathering on it and can be seen in the southwestern and northwestern portion of the area investigated.

Areas that are underlain by older and younger metasediments rock units shows moderate degree of fracturing and weathered layer thickness compare to that of the Pan-Africa granites (Figure 2 and 6), thus more promising for groundwater development (see figure 5).



**Figure 4.** Fractured Thickness Map of the Study Area

The results of weathered layer thickness and fractured thickness were used to produce a groundwater potential map for the studied area (figure 5), based on the notable fact that where there is high thickness of weathered layer overlying fractured layer represent plausible zone for good or excellent groundwater potential. From the figure 3 and 6, it is clear that H type curves and KH type curves denote areas for an excellent groundwater prospect. Comparing this result with the lineament map of the studied area

in figure 7 it become obvious that the area that exhibits high degree of fracturing tends to have more plausible tendencies of forming excellent water saturated aquifer. Wells or boreholes that penetrated this horizon can usually provide sufficient water to sustain even hand-pump.

This lend credence that proper rating of curve-type obtained from VES data interpretation could be used to decipher area for groundwater potential.

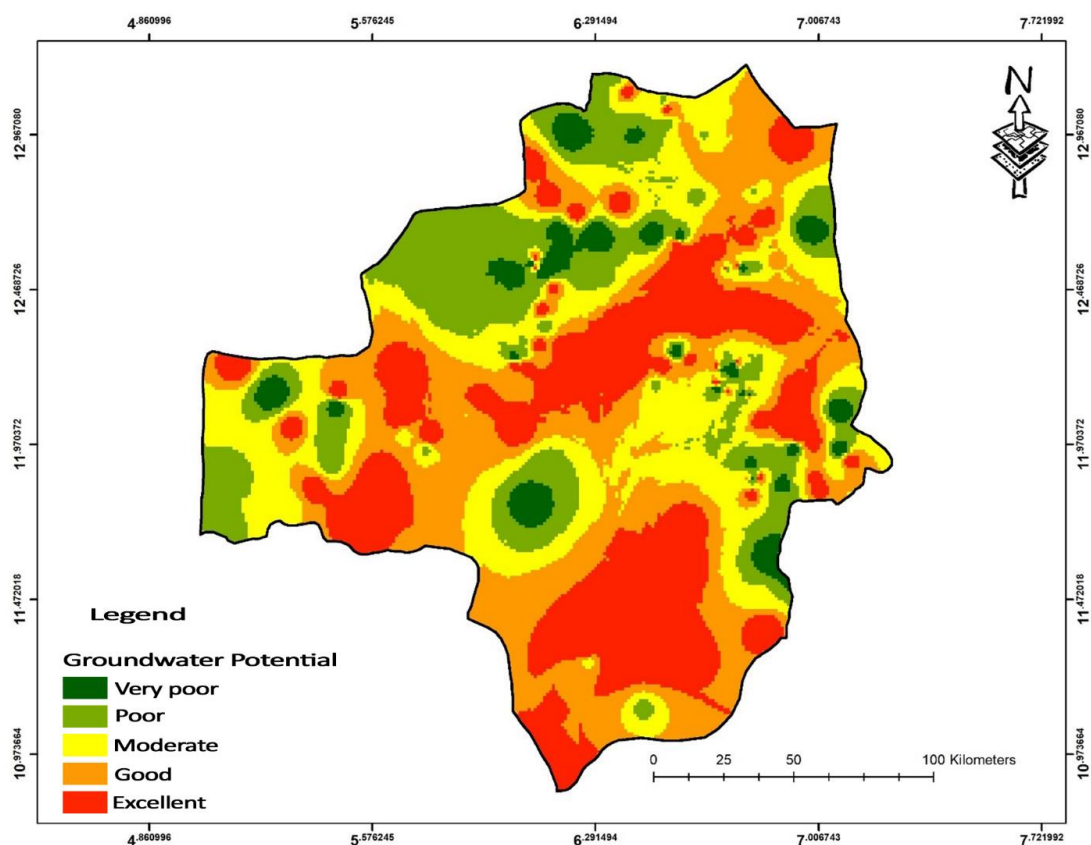


Figure 5. Groundwater Potential Map

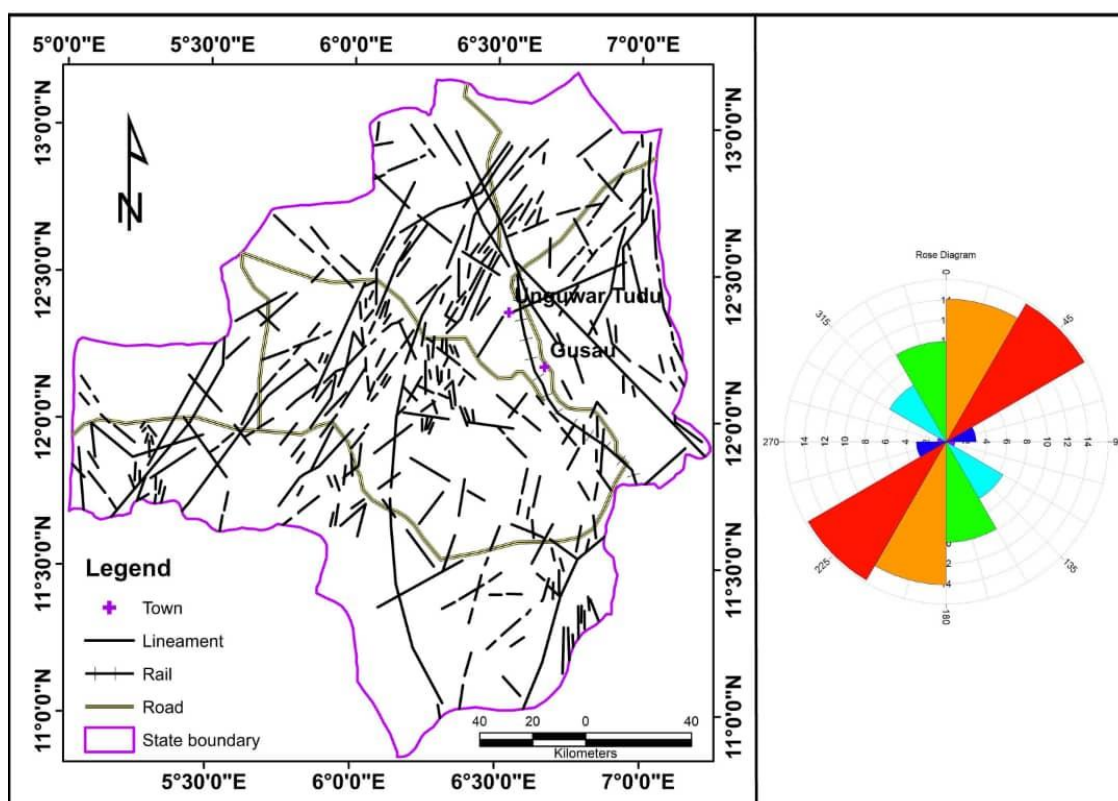


Figure 6. Lineament Map of the Study Area

## 5. Evaluation of Dar Zarrouk Parameters within the Sedimentary Section of the Study Area

The reflection coefficient ( $R_c$ ) is a measure of the degree of fracture in an area. It could also indicate the density of formation in the aquifer. Areas of low reflection coefficient value have high water potentials (table 5). The reflection coefficient ( $R_c$ ) values obtained from sedimentary rock formation of the studied area range between 0.01 to 1.00 with mean value of 0.65 which suggest excellent groundwater

potential compare to the aquifers of the studied basement complex (table 6).

Low values of resistivity contrast indicate high groundwater potentials. The values of resistivity contrast obtained from the VES data within the Gundumi formation range from 0.01 to 30.73, this suggest an excellent level of groundwater potential.

Low value of coefficient anisotropy ( $\lambda$ ) may be indicating high-density water-filled aquifer. In this work the value of coefficient anisotropy obtained from sedimentary rock unit (Gundumi formation) range from 0.44 to 3.79, this values implies moderate density-filled aquifer.

**Table 5.** Evaluation of Dar-Zarouk Parameters

| VES Locations | Reflection Coefficient ( $R_c$ ) | Resistivity Contrast ( $F_c$ ) | Longitudinal Resistivity ( $\rho_L$ ) | Transverse Resistivity ( $\rho_t$ ) | Coefficient Anisotropy ( $\lambda$ ) |
|---------------|----------------------------------|--------------------------------|---------------------------------------|-------------------------------------|--------------------------------------|
| 1             | 0.137                            | 0.759                          | 113                                   | 131                                 | 1.077                                |
| 2             | 0.069                            | 1                              | 144.68                                | 189                                 | 1.143                                |
| 3             | 0.28                             | 0.563                          | 32.68                                 | 43                                  | 1.145                                |
| 4             | 0.878                            | 15.45                          | 38.1                                  | 201                                 | 2.296                                |
| 5             | 0.389                            | 0.439                          | 41.6                                  | 45                                  | 1.038                                |
| 6             | 0.7                              | 0.176                          | 72                                    | 78.89                               | 1.047                                |
| 7             | 0.121                            | 0.784                          | 94.83                                 | 125                                 | 1.147                                |
| 8             | 0.842                            | 11.64                          | 36.73                                 | 238.8                               | 2.549                                |
| 9             | 0.177                            | 1.434                          | 41.23                                 | 265.39                              | 2.535                                |
| 10            | 0.0095                           | 1.019                          | 58.2                                  | 155                                 | 1.632                                |
| 11            | 0.796                            | 8.77                           | 10.82                                 | 38.2                                | 1.879                                |
| 12            | 0.734                            | 6.53                           | 38.08                                 | 160.88                              | 2.055                                |
| 13            | 0.671                            | 5.096                          | 73.65                                 | 83.2                                | 1.062                                |
| 14            | 0.988                            | 16.05                          | 106.81                                | 2798                                | 5.12                                 |
| 15            | 0.999                            | 0                              | 61.43                                 | 98.5                                | 1.27                                 |
| 16            | 0.923                            | 0.03                           | 76.39                                 | 160.42                              | 1.449                                |
| 17            | 0.956                            | 45                             | 22.25                                 | 306                                 | 3.687                                |
| 18            | 0.937                            | 30.75                          | 37.78                                 | 1507                                | 6.318                                |
| 19            | 0.348                            | 0.50                           | 6.7                                   | 703                                 | 10.24                                |
| 20            | 0.783                            | 0.12                           | 52.2                                  | 285.11                              | 2.337                                |
| 21            | 0.93                             | 0.04                           | 46                                    | 477                                 | 3.205                                |
| 22            | 854                              | 0.08                           | 27                                    | 386                                 | 3.786                                |
| 23            | 0.871                            | 0.07                           | 71.32                                 | 146.59                              | 1,433                                |
| 24            | 0.82                             | 0.10                           | 85.6                                  | 83.79                               | 0.989                                |
| 25            | 0.987                            | 0.01                           | 40                                    | 346.75                              | 2.946                                |
| 26            | 0.806                            | 0.11                           | 44                                    | 94.21                               | 0.743                                |
| 27            | 0.869                            | 0.07                           | 81.421                                | 192.21                              | 0.994                                |
| 28            | 0.974                            | 0.01                           | 69.98                                 | 100.58                              | 1.199                                |
| 29            | 0.692                            | 0.18                           | 66.11                                 | 75.7                                | 1.07                                 |
| 30            | 0.619                            | 4.25                           | 105                                   | 267.5                               | 1.595                                |
| 31            | 0.495                            | 2.96                           | 89.44                                 | 354                                 | 1.989                                |
| 32            | 0.482                            | 2.814                          | 71.44                                 | 289                                 | 1.56                                 |
| 33            | 0.838                            | 0.088                          | 28.1                                  | 274                                 | 3.12                                 |
| 34            | 0.495                            | 2.963                          | 89.44                                 | 354                                 | 1.989                                |
| 35            | 0.262                            | 0.584                          | 92                                    | 22.31                               | 0.492                                |
| 36            | 0.781                            | 8.16                           | 88                                    | 119                                 | 1.164                                |
| 37            | 0.495                            | 2.96                           | 43.21                                 | 78.51                               | 1.347                                |



|    |       |       |        |       |       |
|----|-------|-------|--------|-------|-------|
| 38 | 0.838 | 0.088 | 62.41  | 94.71 | 1.231 |
| 39 | 0.84  | 11.51 | 178.21 | 394   | 1.486 |

## 6. Conclusion

Groundwater potential assessment was carried out in Zamfara State, Northwestern Nigeria. A total of one hundred and eighty-three (183) vertical electrical soundings (VES) were used to identify potential groundwater bearing zones capable of sustaining economic development and potential growth of the study area. Two hydrogeological units were investigated (basement rock units and sedimentary rock unit). The qualitative and quantitative interpretations have helped in the delineating aquifer zones in the study area.

Generally, the VES result from the basement rock units revealed, four to five geoelectric layers which correspond to lateritic top soil, weathered basement (clay), partially fractured layer, fractured layer and fresh basement. The weathered/fractured layer was identified as the water bearing layer within the basement rock units of the study area. South-northeastern zone tends to be the most prospective region with the best hydrogeologic conditions for borehole siting.

Hydro-resistivity parameters evaluated from the basement rock units showed that the sounded locations have good groundwater potential that can sustain households (domestic water use).

Consequently, three geoelectric layers were delineated from VES result from sedimentary formation (section of the study area), which includes sandy clayey top/gravel sandy top soil, second layer are mostly silty clay/compacted laterite/compacted sandstone/sandy gravels layers, the third layer were majorly sandstone in some instances silty clay. However, the aquiferous layer is saturated sandstone/sandy gravel layer.

The Dar Zarrouk results revealed excellent groundwater potential within this formation. The values of coefficient anisotropy obtained from sedimentary rock unit range from 0.44 to 3.79, this signifies moderate groundwater density. Though, the values obtained from basement rock units were much high. This is concluded that the aquifers of the Gundumi formation is more promising and it can be tap for both domestic and agricultural use.

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## Conflict of interest

There is no conflict of interest.

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